CITY OF GREELEY COMPREHENSIVE DRAINAGE PLAN

GREELEY NO. 3 DITCH FINAL SUMMARY HYDRAULICS REPORT

Prepared for:

City of Greeley Public Works Department 1001 Ninth Avenue Greeley, CO 80631

Prepared by:

Anderson Consulting Engineers, Inc. 772 Whalers Way, Suite 200 Fort Collins, CO 80525 (ACE Project No. COCOG05)

March 8, 2006



March 8, 2006

Mr. Bert Leautaud City of Greeley Public Works Department 1001 Ninth Avenue Greeley, CO 80631

City of Greeley Comprehensive Drainage Plan – Greeley No. 3 Ditch RE:

(ACE Project No. COCOG05)

Dear Bert:

Anderson Consulting Engineers, Inc. (ACE) is pleased to inform you that we have completed the analyses and documentation associated with the hydraulic evaluation of the Greeley No. 3 Ditch. In addition, we have completed all revisions to the report pursuant to City review comments and our final in-house review. Please find enclosed two copies of the Final Summary Hydraulics Report along with all accompanying backup documentation.

It has been our pleasure working with you toward the completion of this study. If you have any questions or comments concerning the Report, please do not hesitate to contact us.

Sincerely,

Anderson Consulting Engineers, Inc.

Gregory J. Koch, P.E. Vice President

Brian L. Van Zanten, P.E.

Project Engineer II

GJK/BLV/vla

Enclosures

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I. INTRODUCTION

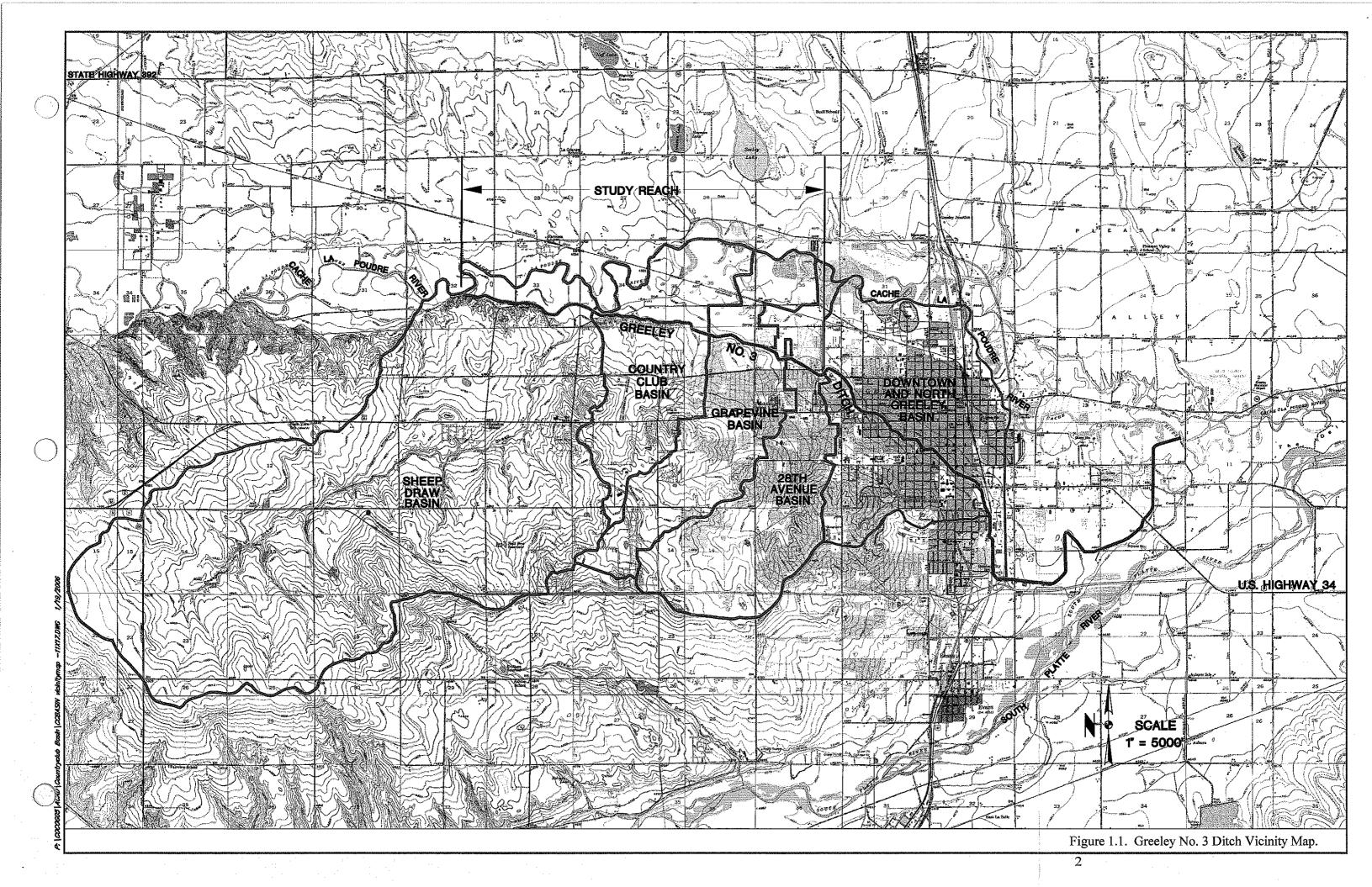
1.1 Background

The Greeley No. 3 Ditch is an irrigation facility that transports both irrigation flows and stormwater flows through the City of Greeley. A manually controlled headgate directs flow into the ditch at the Cache la Poudre River (approximately 0.6 miles west of the intersection of 71st Avenue and F Street) and also has its terminus at the Cache la Poudre River (immediately north of 16th Street and west of Fern Avenue, just outside of the Greeley city limits), a length of approximately 12 miles. The ditch generally flows in a southeasterly direction, traversing five of the City's major drainage basins. A vicinity map depicting the alignment of the Greeley No. 3 Ditch is provided in Figure 1.1.

This study is restricted to the reach west of 23rd Avenue, specifically beginning at the headgate to the Cache la Poudre River as the upstream limit and the Clarkson Spill Structure serving as the downstream limit. This reach of the ditch spans four out of the five City's major drainage basins, including the Sheep Draw Basin, the Country Club Basin, the Grapevine Basin, and the 28th Avenue Basin. The reach of the ditch east of the Clarkson Spill Structure to immediately upstream of the U.S. Highway 85 Bypass was studied in detail as part of the Downtown and North Greeley Basin (Anderson Consulting Engineers, Inc., January 2005); detailed analyses related to that reach are found in that report.

The ditch has several turnouts for diverting irrigation flows, as well as four controlled spill structures for the release of excess stormwater flows located within the Country Club Basin, Grapevine Basin, and 28th Avenue Basin. At several locations, the capacity of the ditch is compromised due to constrictions at bridge or culvert crossings, flow measurement structures, or pipeline crossings. Such encroachments increase the potential for ditch spills. The ditch had not been formerly identified as a north-south drainage boundary in previous Comp Planning efforts. Based on recent analyses, however, the ditch does effectively function as a drainage boundary in the Country Club and Grapevine Basins where the ditch intercepts and conveys either all runoff or a significant portion of the runoff from storm events as large as that associated with the 100-year return period. However, while the ditch serves as a significant drainage boundary through the Country Club and Grapevine Basins, it does not effectively function as a drainage boundary in the Sheep Draw and 28th Avenue Basins. Uncontrolled left bank overtopping generally occurs within the Sheep Draw and 28th Avenue Basins for flows as small as those associated with a 5-year return period.

Within the current study reach, the ditch maintains the following three important functions: (1) conveying irrigation flows to various locations within and in the vicinity of the



City of Greeley; (2) intercepting storm runoff from areas south of the ditch; and (3) depending upon location and magnitude of the inflows, safely evacuating those flows through the four controlled spill structures, located west of 23rd Avenue. Historically, larger inflows (e.g., flows associated with a 50-year return period and higher) had a tendency to greatly exceed the capacity of the ditch. As a result, uncontrolled, localized bank overtopping occurred at many locations; particularly both east and west of 59th Avenue in the Sheep Draw Basin, west of 35th Avenue in the Grapevine Basin, and both north and south of 4th Street in the 28th Avenue Basin. Beyond these five general areas, uncontrolled bank overtopping within the four subject drainage basins was relatively limited and isolated.

The City has recently implemented numerous regional drainage improvements and imposed local drainage requirements to reduce stormwater flows entering the ditch by means of the following: (1) local detention has been provided by all recent development within the City to minimize releases into the ditch; and (2) regional detention has also been provided upstream of the ditch, which has served to either minimize flows entering the ditch, or bypass the ditch altogether by conveying releases over or under the ditch. In addition, the recent construction of four controlled spill structures aid in the ditch operation by directing stormwater flows that still enter the ditch to dedicated drainage facilities where they can be safely transported away from the ditch. These spill structures have helped to maintain the Greeley No. 3 Ditch as a viable mechanism for the controlled transport of stormwater runoff.

1.2 Previous Studies

The Greeley No. 3 Ditch was studied in detail as part of the efforts associated with the "Comprehensive Drainage Plan Update, City of Greeley, Greeley No. 3 Ditch, Volumes 1 and 2 - Project Notebook," Lidstone and Anderson, Inc., March 1996. Specifically for that study, a comprehensive inventory and survey of ditch cross sections and crossing structures was conducted to document the condition of the existing facilities and identify locations of potential spills. This work was followed by a detailed hydraulic evaluation of the ditch using HEC-2. Structures and reaches of the ditch, which specifically limit the capacity to convey stormwater runoff, were identified. Improvements to divert and/or convey stormwater captured by the ditch were developed and evaluated within the context of the five drainage basins studied as part of the 1997 Comprehensive Drainage Plan. Many of the improvements identified as part of that study have since been implemented, improving the overall effectiveness of the ditch in controlling and conveying stormwater flows.

As mentioned in Section 1.1, the reach of the Greeley No. 3 Ditch from the Clarkson Spill Structure west of 23rd Avenue to just upstream of the U.S. Highway 85 Bypass was studied

in detail as part of analyses related to the Downtown and North Greeley Basin (Anderson Consulting Engineers, Inc., January 2005). That study converted the existing HEC-2 model of the ditch to HEC-RAS, and utilized its unsteady flow capabilities in order to determine outflow spill hydrographs from the ditch. The model was updated as part of the 2005 study to reflect six controlled spill structures as well as associated ditch bank improvements constructed by the City of Greeley since 1997. In addition to these structures and improvements, and to assist in the determination of additional spill locations, lateral weirs were placed between cross sections along the entire left bank of the model. Inflow hydrographs from the hydrologic model that represents the upper portion of the Downtown Basin were input into the hydraulic model, with the hydraulic model being executed under an unsteady flow mode for each return period. Outflow hydrographs at various locations were obtained and consolidated from the hydraulic model and placed back into the hydrologic model that represents the lower portion of the Downtown Basin, as inflow hydrographs. These inflow hydrographs were then utilized to more accurately determine potential flooding locations, and in turn propose drainage improvements for these areas.

1.3 Scope of Work

The Greeley No. 3 Ditch has the potential to significantly alter surface drainage patterns within the limits of the five major drainage basins that contribute stormwater flows to the ditch in the City of Greeley. A detailed evaluation of the ditch that was limited to the Downtown and North Greeley Basin ("City of Greeley, Comprehensive Drainage Plan, Downtown and North Greeley Basin – Final Report, Anderson Consulting Engineers, Inc., January 2005") has already been completed. Comprehensive analyses were not performed on the ditch as part of analysis for the Sheep Draw Basin ("City of Greeley, Comprehensive Drainage Plan, Sheep Draw Basin – Final Report, Anderson Consulting Engineers, Inc., March 2006"). This was due to the limited capacity of the ditch through the basin, the magnitude of potential stormwater inflows entering the ditch at the confluence with Sheep Draw, and the relative hydraulic inefficiency of the existing diversion structure. The ditch is capable of significant, uncontrolled left bank overtopping within the basin limits, and was not foreseen as transferring large amounts of stormwater to the remaining three drainage basins.

The determination of accurate ditch spills (both in location and magnitude) was seen by the City of Greeley as an important part of the overall hydrologic modeling process for the Country Club Basin, Grapevine Basin, and 28th Avenue Basin because of the ability of the ditch to alter drainage patterns and how those flow path alterations can affect drainage improvements

in close proximity to the ditch. The scope of this study identifies the steps utilized in determining those spills, with the specific tasks outlined below.

- 1. <u>Hydrologic Modeling.</u> Existing, Future, and Proposed Condition hydrology was determined for all five drainage basins for the 2-, 5-, 10-, 50-, and 100-year return periods. For the Existing and Proposed Conditions, uniform lateral inflow hydrographs and point inflow hydrographs, for all storm events and scenarios analyzed for this study, were defined as boundary conditions for the ditch based on the results of the hydrologic modeling of the upper portions of the five drainage basins. The unsteady flow hydraulic analyses (described below) were conducted and the resulting spill hydrographs were defined and incorporated into the hydrologic models for the lower portions of the Country Club, Grapevine, and 28th Avenue Basins as inflow hydrographs at the appropriate locations along the downslope side of the ditch.
- 2. <u>Hydraulic Modeling</u>. Unsteady inflow hydrographs from the hydrologic models for each return period were entered into the hydraulic model for the Greeley No. 3 Ditch at various locations. The HEC-RAS model was executed using the unsteady flow routine in order to determine the magnitude and location of ditch spills specific to the Country Club, Grapevine, and 28th Avenue Basins. At the request of the City, however, only the Existing and Proposed Condition scenarios were modeled using HEC-RAS. Unsteady flow analyses were not conducted for the Future Condition as that is a scenario that simply represents an intermediate step between the Existing and Proposed Conditions.
- 3. Integration of Ditch Spills. Pursuant to the results of the HEC-RAS unsteady flow analyses of the Greeley No. 3 Ditch, unsteady outflow/spill hydrographs were determined for the Existing and Proposed Condition for the Country Club, Grapevine, and 28th Avenue Basins for all five return periods. The hydrographs were entered into each corresponding hydrologic model at the appropriate location. It is noted that for the Future Condition hydrology models, the Existing Condition outflow hydrographs from the ditch to the lower portion of the basins were utilized. It is recognized that assuming Existing Condition inflow hydrographs are applicable in the Future Condition models may result in slightly under-estimated (for both the Country Club and 28th Avenue Basins) or overestimated (Grapevine Basin) peak discharges north of the ditch. This was deemed as an acceptable compromise by City staff in order to simplify the analyses for the Future Condition.

II. HYDROLOGIC ANALYSES: MODELING APPROACH AND INFLOW HYDROGRAPHS

2.1 Existing Condition

The Existing Condition scenario was defined as existing development with existing facilities for the five major drainage basins. Existing development was defined on a basin-by-basin basis, depending upon when the development had been approved for construction by the City of Greeley. Storm hydrographs for each return period were determined using the Colorado Urban Hydrograph Procedure (CUHP). After a conversion program converted the CUHP hydrographs into EPA SWMM hydrographs, the flows were entered into each model and in turn routed within each basin using EPA-SWMM. The resulting hydrographs specifically contributing runoff to the ditch were then extracted from the SWMM models and tabulated for use within the Greeley No. 3 Ditch HEC-RAS model.

2.2 Future Condition

The Future Condition scenario was defined by modifying the Existing Condition model to incorporate all potential future development based on current zoning and land use. The model also assumed that all existing major drainage facilities (generally located along major drainageways within each basin) would be retained from the Existing Condition. At the request of the City, Future Condition hydrographs were not utilized for any hydraulic analyses on the ditch. This determination was based on the fact that since nearly 90 percent of the four basins contributing flow to the ditch (excluding Sheep Draw) had already been developed prior to Future Condition modeling efforts, inflow hydrographs to the ditch were similar for the two conditions. It is noted that assuming Existing Condition inflow hydrographs north of the ditch are applicable to the Future Condition may result in either a slight under-estimation or overestimation (depending on the drainage basin of interest) of peak discharges.

2.3 Proposed Condition

The Proposed Condition scenario incorporated all Future Condition modeling efforts and included proposed improvements generally along the major drainageways within each basin. In short, the objective of the Proposed Condition modeling efforts was to mitigate potential flooding problems and more importantly from a ditch perspective, reduce flows contributing to

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III. HYDRAULIC ANALYSES

3.1 Hydraulic Model Modifications

The hydraulic (HEC-2) model for the Greeley No. 3 Ditch that was prepared as part of the 1997 Comp Plan was converted to HEC-RAS as part of the 2005 Comp Plan. The reach beginning near the downstream end of the original model (immediately upstream of the U.S. Highway 85 Bypass) and continuing upstream nearly to the Clarkson Spill Structure (west of 23rd Avenue) was recently converted to HEC-RAS Version 3.1.2 for the Downtown and North Greeley Basin analyses (Anderson Consulting Engineers, Inc., January 2005). The remainder of the ditch (from the Clarkson Spill Structure up to the headgate at the Cache la Poudre River) was converted to HEC-RAS Version 3.1.2 and 3.1.3 for analyses relating to the Country Club Basin, Grapevine Basin, and 28th Avenue Basin; these two reaches were then connected, producing a single hydraulic model for the entire ditch. For purposes of analyses related to all three basins, it was assumed that only normal irrigation flows (70 cfs) would enter the Greeley No. 3 Ditch from the Poudre River.

Modeling parameters for bridges and culverts were modified to accommodate improved modeling techniques available in HEC-RAS; however, these modifications were based on geometric information gathered as part of the 1997 Comp Plan efforts. The ditch was not resurveyed as part of the current study; consequently, inherent in this analysis is the assumption that the previously defined cross sectional data for the ditch provides a reasonably accurate hydraulic representation of existing conditions. The exception to the use of previously defined geometric ditch data is the incorporation of the left (downslope) ditch bank spill structures constructed since they were recommended as part of the 1997 Comp Plan. Ditch bank data were modified in the hydraulic model based on design drawings of the two new spill structures west of 23rd Avenue. In addition to the new spill structures, ditch bank data were modified to reflect recent improvements to the two existing spill structures west of 23rd Avenue. The four spill structures were designed and/or modified to improve the efficiency of stormwater removal.

Beginning at the upstream end of the ditch, the first spill structure to be improved was the F Street Spill Structure, located in the northwest corner of the Country Club Basin approximately 0.3 miles east of the intersection of F Street and 59th Avenue. Improvements were first outlined for this structure as part of the 1997 Comp Plan efforts, which called for extending the side channel weir upstream along the left bank to divert a maximum discharge of 160 cfs north to the Cache la Poudre River through the existing wasteway structure, limiting the stormwater captured by the ditch to less than 100 cfs downstream of the diversion structure. In conversations with City staff and as part of the updated design, the structure is intended to maintain approximately 110 cfs in the ditch by means of controlled spills over the extended side channel weir and

through a single steel crest gate controlled by an automated assembly. As previously planned, the structure was extended upstream along the left bank of the No. 3 Ditch with a concrete side channel weir, and tied into the existing wasteway structure. The improved diversion structure is depicted in Figure 3.1.

Further downstream along the ditch, the second spill structure to be constructed as part of the 1997 Comp Plan recommendations was Eagleview Side Channel Weir, built in conjunction with the improvements made as part of the South Eagleview Detention Pond. The pond is located near the northeast corner of the Country Club Basin, north of the intersection of B Street and 43rd Avenue Court, south of the Greeley No. 3 Ditch. The 1997 plan called for a flume to be constructed over the



Figure 3.1 F Street Spill Structure.

ditch, routing flows from the Larson Ditch into a regional detention pond to be built immediately north of the ditch. A side channel weir was also included, intending to spill all flows in excess of 100 cfs into the pond from the ditch. The revised plan depicts the Larson Ditch directing flows into the pond south of the ditch, with pond outflows flumed over the ditch via a spillway and combined with flows from the side channel weir into a drainage channel. A 12'Wx3'H RCB (reduced to 9 feet in width due to an orifice plate) was installed along the ditch centerline

immediately downstream of the side channel weir in order to accommodate the pond outflow flume and to force excess stormwater flows over the weir. The drainage channel directs flows to the north into a second regional pond between F Street and the Colorado and Southern Railroad. The Greeley No. 3 Ditch, concrete side channel weir, and pond outflow spillway are portrayed in Figure 3.2.

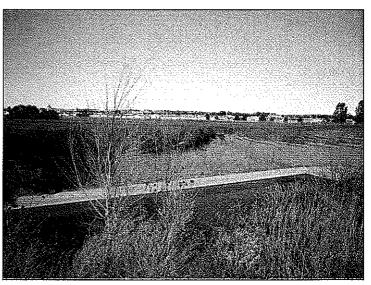


Figure 3.2 Eagleview Side Channel Weir and Pond Outflow Spillway.

The third spill structure recommended as a result of the 1997 Comp Plan was the Northview Side Channel Weir; this structure was built in conjunction with the improvements made as part of the Northview Regional Detention Pond. The pond is located near the northwestern corner of the 28th Avenue Basin, northeast of the intersection of 30th Avenue and

4th Street, north of the Greeley No. 3 Ditch. Improvements outlined for this structure as part of the 1997 Comp Plan included a flume over the ditch, routing flows from the Grapevine Basin secondary drainageway into a regional detention pond to be built immediately north of the ditch. A concrete side channel weir was also designed to spill all flows in excess of 100 cfs into the pond. As part of the design, pond outflows were intended to flow back to the west to the 35th Avenue Outfall Channel. The revised plan portrays the



Figure 3.3 Northview Side Channel Weir, In-line Ditch Control Structure, and Ditch Underchute.

pond to the north of the ditch as planned, with secondary drainageway flows routed beneath the ditch via an underchute. Underchute flows are combined with flows from the side channel weir. An in-line ditch control structure, also constructed in the Greeley No. 3 Ditch as part of the improvements, was installed immediately downstream of the side channel weir. Located directly downstream of the side channel weir, this structure is intended to force higher flows to spill over the side channel weir by means of stop logs placed within the top half of the ditch control structure section. Once flows have been directed into the pond, pond outflows are routed to the northeast toward the Greeley No. 3 Ditch Wasteway. The Northview improvements are shown in Figure 3.3.

The fourth and final spill structure to be improved was the Clarkson Spill Structure, located at the basin boundary between the 28th Avenue Basin and the Downtown and North Greeley Basin. The structure is located immediately south of the intersection of 4th Street and 25th Avenue. Proposed improvements as part of the 1997 Comp Plan called for automation of the structure so as to divert stormwater flows in excess of 80 cfs into the Greeley No. 3 Ditch Wasteway. The revised design included reconstruction of the structure to include a single overshot gate for the diversion of stormwater flows to the north into the Greeley No. 3 Ditch Wasteway. The design also included an automation assembly to maintain approximately 110 cfs in the ditch, according to conversations with City staff. The rehabilitated structure is represented

in Figure 3.4. Design/rehabilitation plans for each of the four spill structures are provided in Appendix A.

The Downtown and North Greeley Basin also included the addition of several spill structures and improvements designed constructed as part of the 1997 Comp Plan. A more detailed discussion of those structures may be found in the Downtown and North Greeley Basin report (Anderson Consulting Engineers, Inc., January 2005).

Lateral weirs were defined along the entire length of the left (downslope) bank through all five basins. These weirs included the



Figure 3.4 Clarkson Spill Structure.

controlled spill structures. Where bank improvements have not been implemented, lateral weirs were defined based on top of left bank elevations provided in the original HEC-2 model.

3.2 Unsteady Flow Modeling

Seventeen uniform lateral inflow hydrographs and twelve lateral inflow hydrographs, for all storm events and scenarios analyzed for this study, were defined as boundary conditions for the ditch. These inflows were defined based on the results of the hydrologic modeling of the upper portions of the five major basins. Three additional boundary conditions were included, and they are listed as follows:

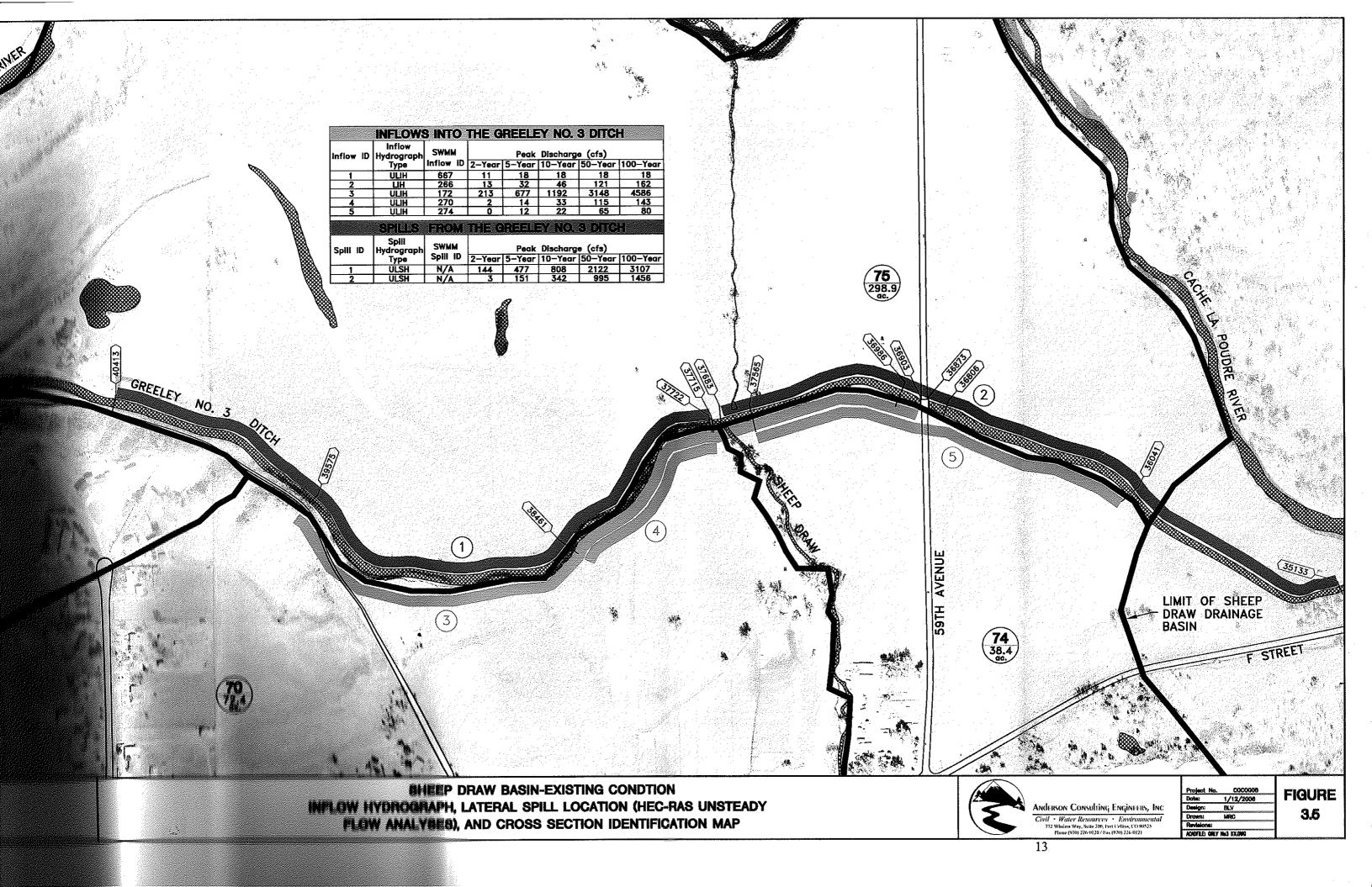
- 1) A steady inflow hydrograph of 70 cfs was entered at the upstream end of the model to simulate normal irrigation flows;
- 2) An in-line ditch control structure (installed as part of the Northview Regional Detention Pond improvements, and depicted in Figure 3.3) was placed immediately downstream of the Northview Side Channel Weir to simulate a maximum gate height opening of 2.67 feet; and
- 3) A normal depth slope of 0.02 ft/ft was assumed at the downstream end of the model.

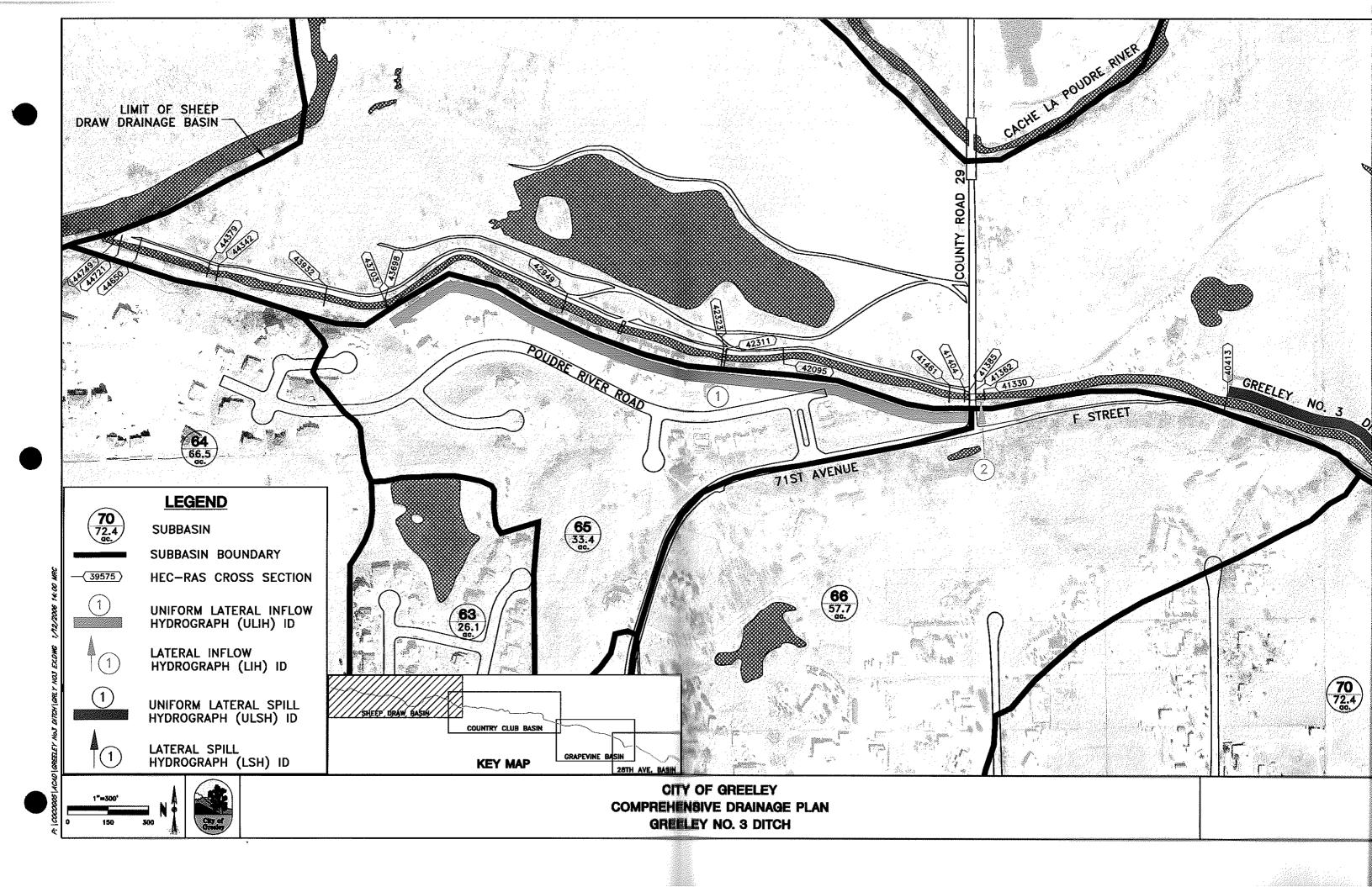
It should also be noted that at the F Street Spill Structure and the Clarkson Spill Structure, discharge rating curves were established at each location. This was done to effectively maintain 110 cfs in the ditch downstream of each structure. Site-specific analyses were conducted at each location; the results of these analyses indicated that each structure has the capability to limit downstream flows along the ditch to 110 cfs if operated properly. HEC-RAS does not have the capability to model an automated gate designed to maintain specific water surface elevations within the ditch; therefore, discharge rating curves were developed and entered into the model. The unsteady flow analyses were conducted for both the Existing and Proposed Condition. Resulting spill hydrographs were defined and incorporated into the hydrologic models for the lower portion of the basin as inflow hydrographs at the appropriate locations along the downslope side of the ditch.

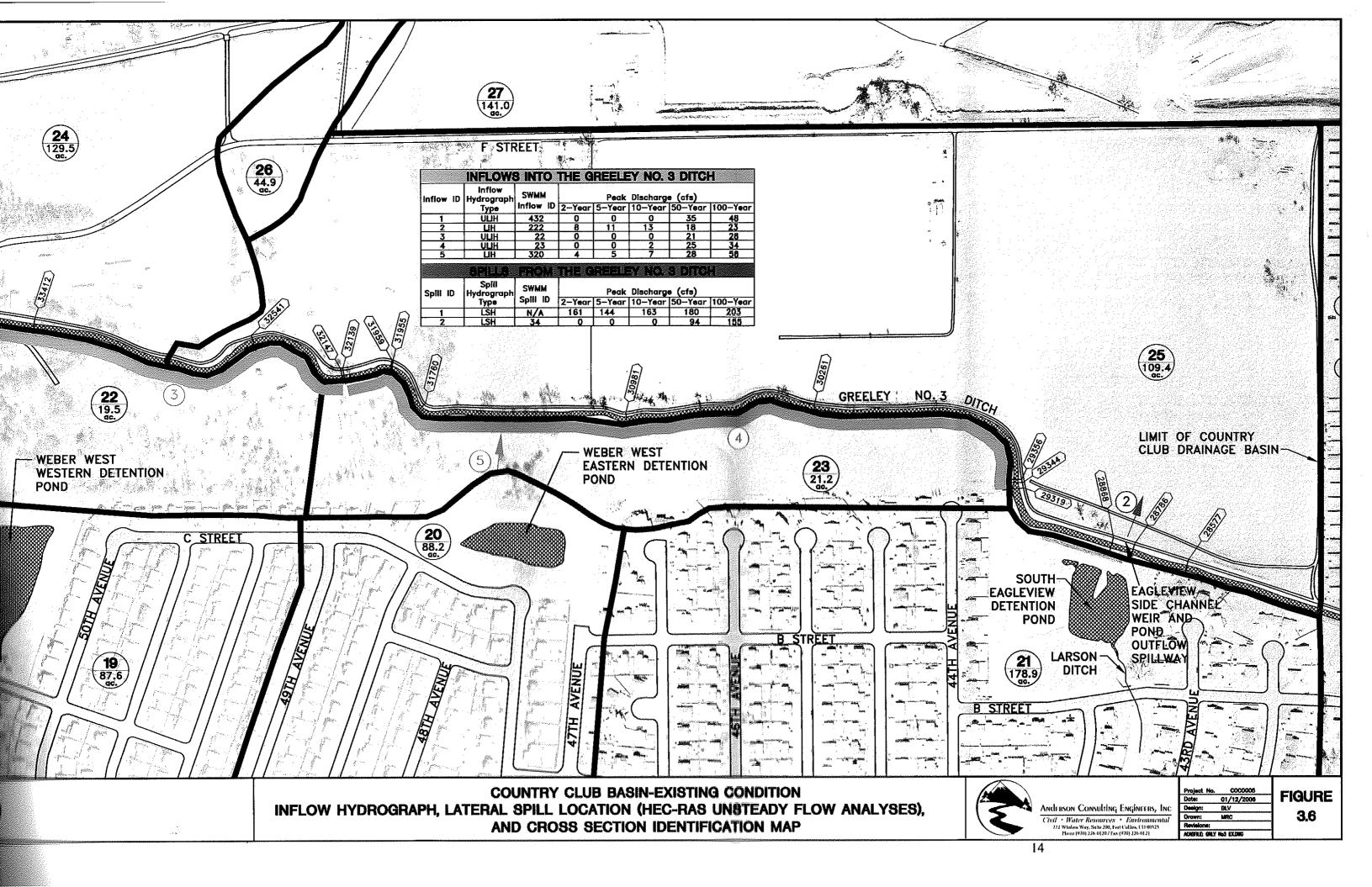
3.2.1 Hydraulic Modeling Results from the Existing Condition Unsteady Flow Model

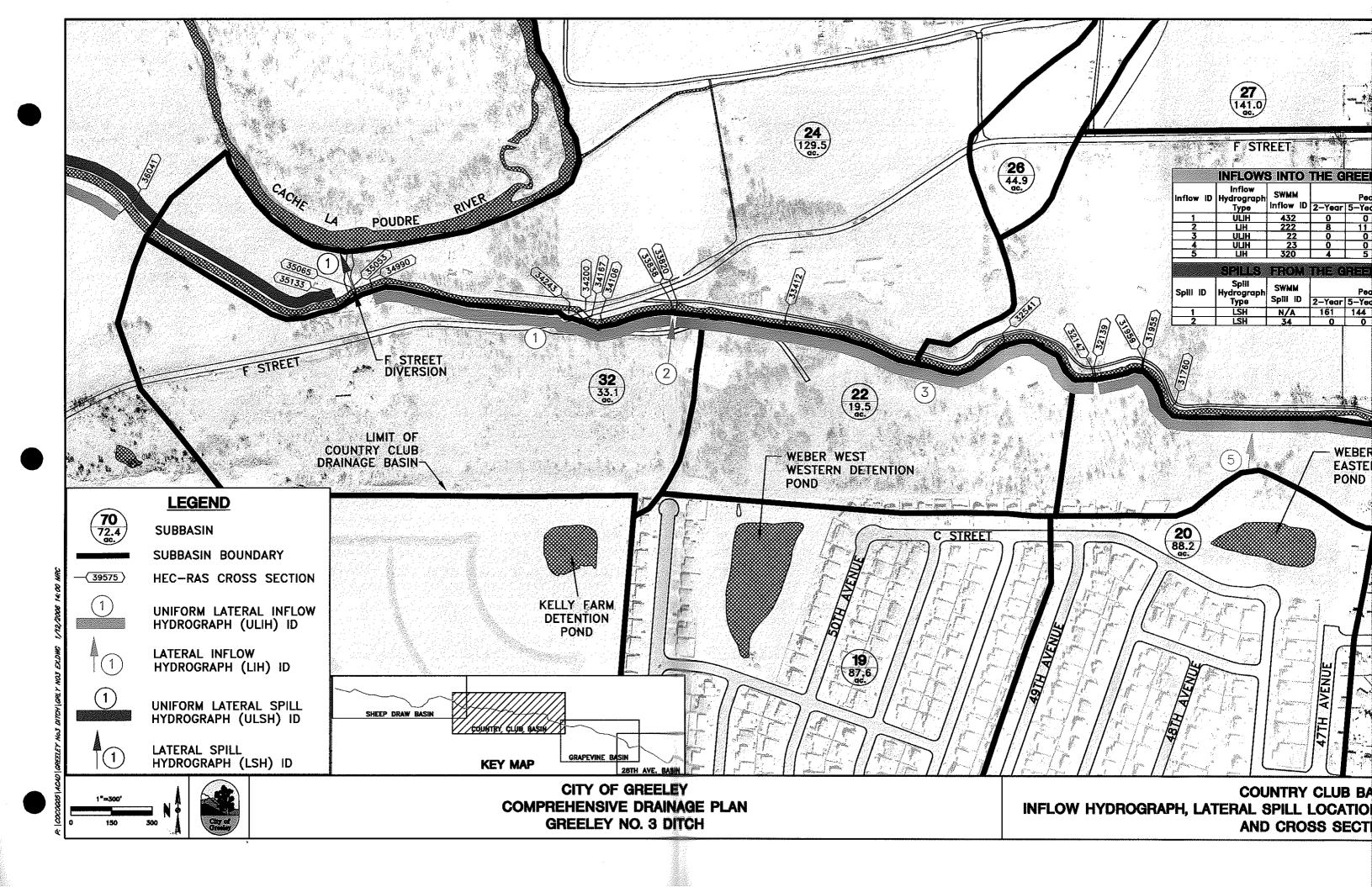
The Existing Condition analyses for the four major drainage basins indicate that within the Country Club and Grapevine Basins, the ditch is generally effective in controlling bank overtopping and only spilling at the controlled spill structures for storms up to and including a 100-year event. The one exception is uncontrolled, left bank overtopping immediately west of 35th Avenue in the Grapevine Basin during the 100-year event. Uncontrolled bank overtopping is a significantly larger concern within the limits of the 28th Avenue Basin for storms at a 5-year event and higher. Figures 3.5 through 3.8 depict the limits of the Greeley No. 3 Ditch (on aerial photographs taken in 2003) through the Sheep Draw, Country Club, Grapevine, and 28th Avenue Basins. Included in these figures are cross section locations, inflow hydrograph types and approximate spill limits, and tabular information depicting the following: (a) inflow hydrograph and spill identification numbers; (b) inflow and spill hydrograph types (Uniform Lateral or Lateral Inflow Hydrographs, and Uniform Lateral or Lateral Spill Hydrographs, respectively), (c) SWMM inflow and spill/outflow node numbers as they relate to the hydrologic models, if applicable; and (d) peak spill discharges for the five return periods. It is noted that tabular summaries of inflow and outflow/spill hydrographs through the Downtown and North Greeley Basin have already been provided for the ditch in Section 3.4 of the Project Notebook associated with that basin.

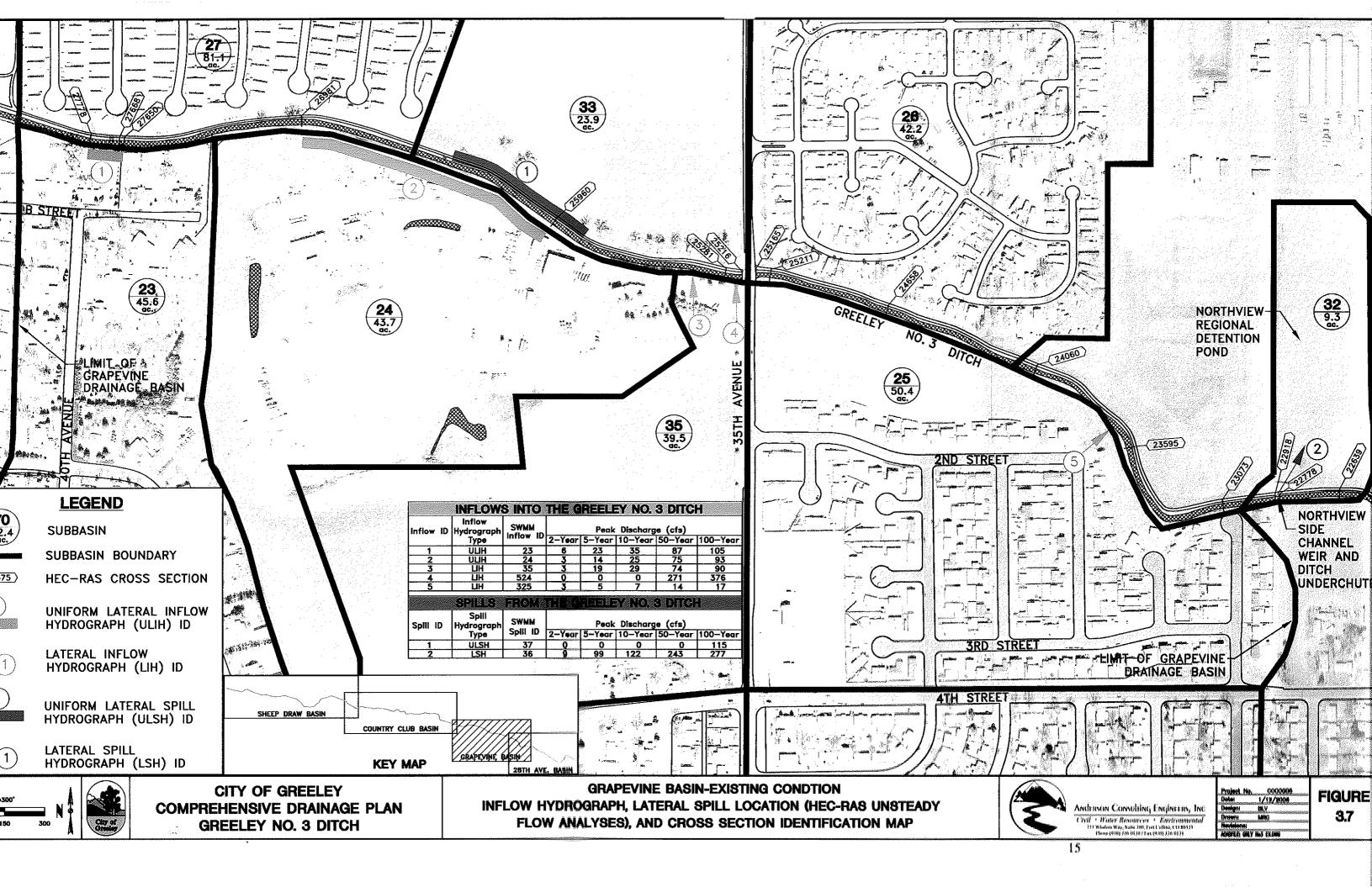
Analyzing the ditch on a basin by basin basis, uncontrolled, left bank overtopping of the ditch is prevalent through the Sheep Draw Basin for all return periods from approximately F Street (west of the intersection of the ditch and Sheep Draw) to the eastern limit of the basin (east of 59th Avenue). Ditch spills in this area are seen as having minimal consequence due to lack of development between the ditch and the Poudre River and the presence of the Poudre River

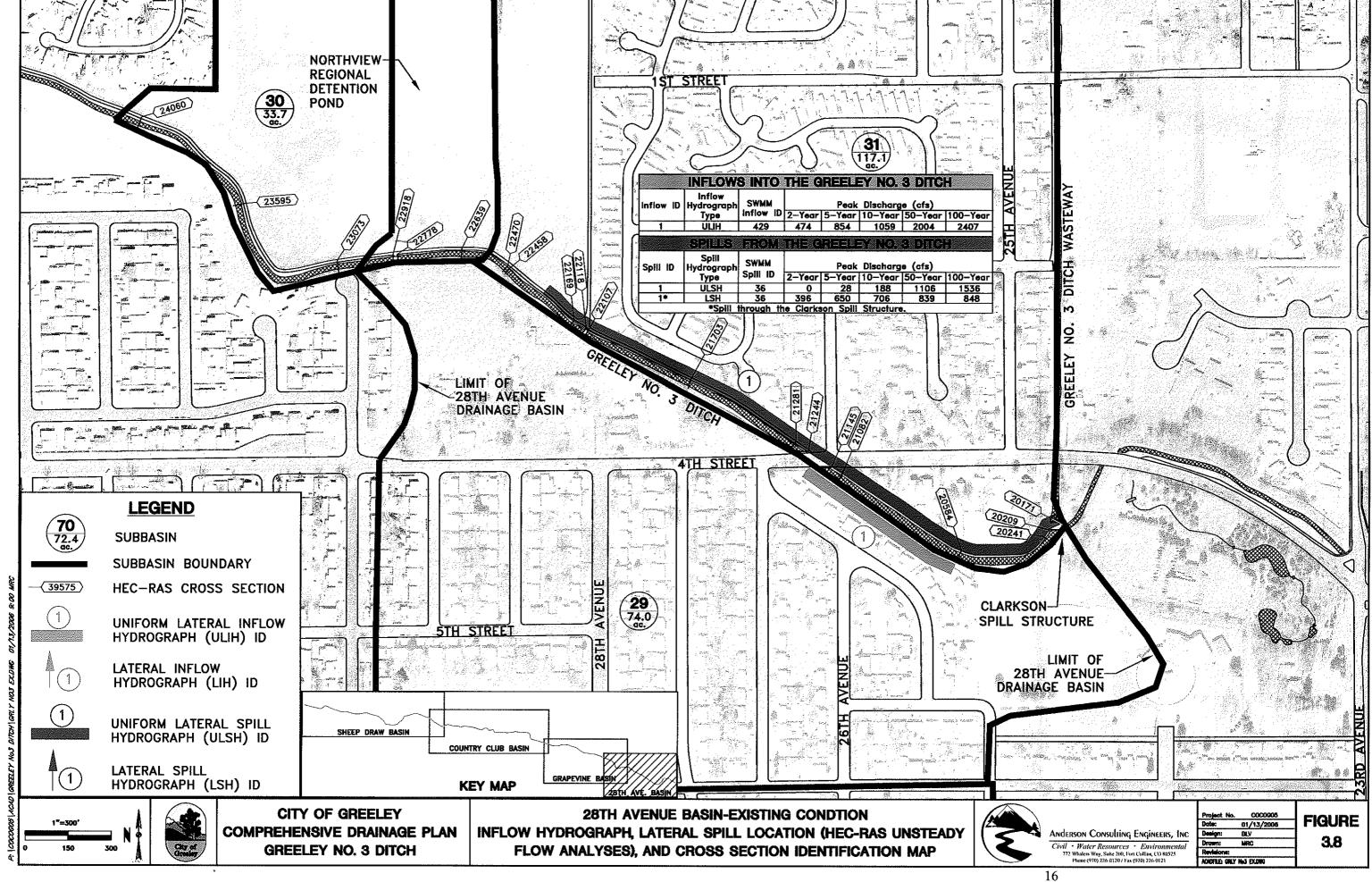










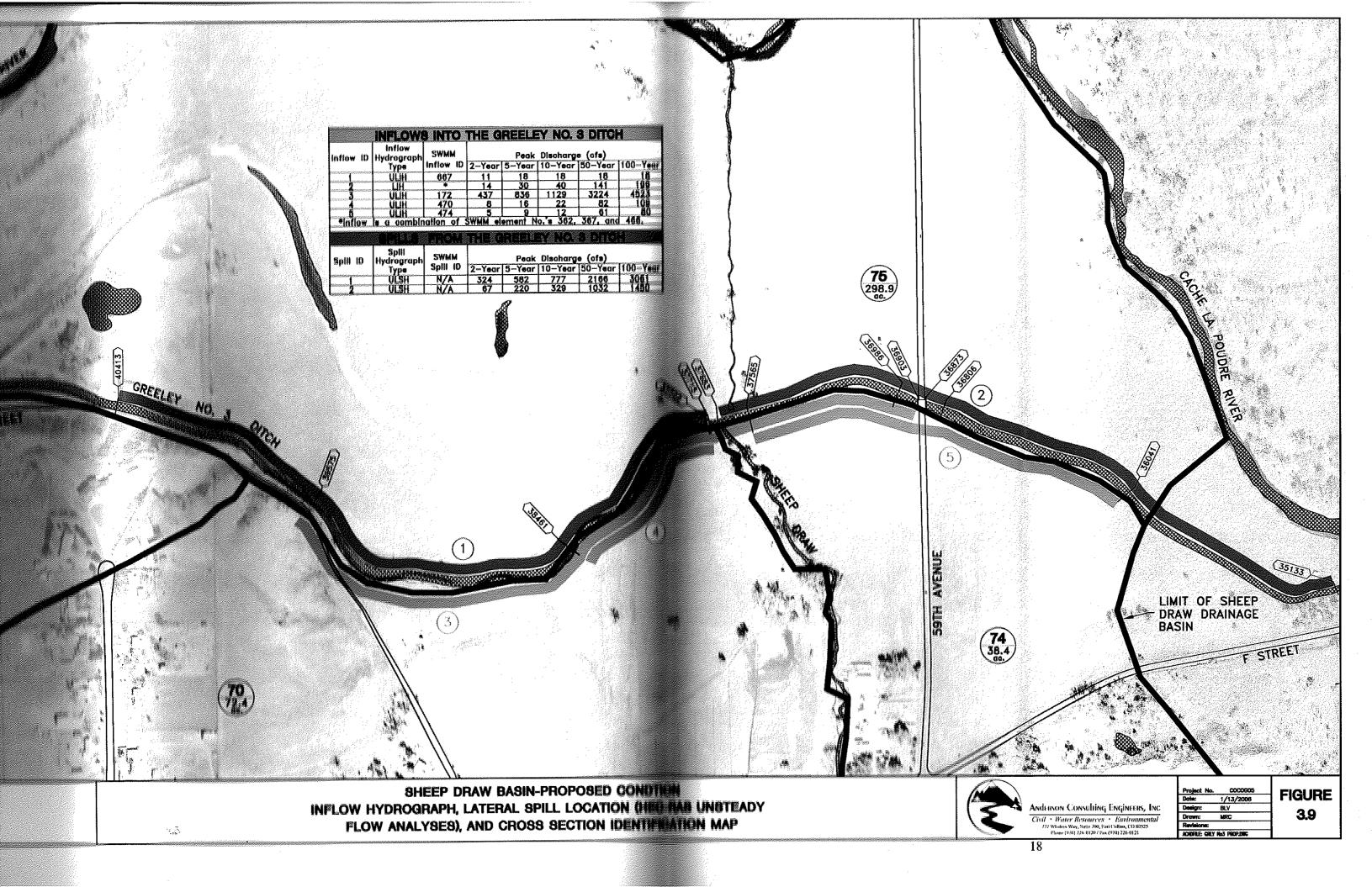


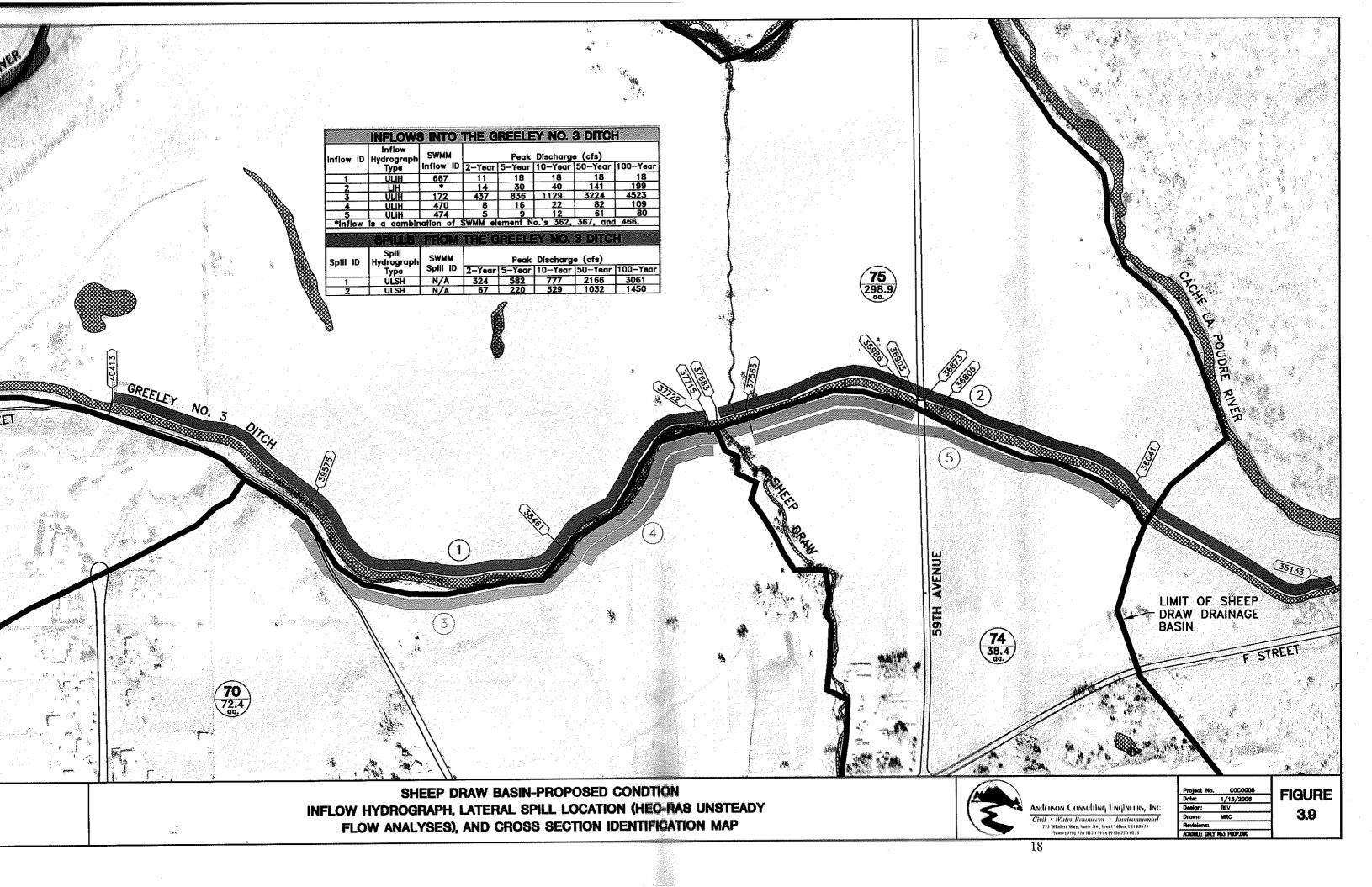
floodplain, which encompasses this area. Ditch spills are confined to the two spill structures (F Street and Eagleview) within the Country Club Basin; according to the unsteady flow analyses, the Eagleview Side Channel Weir does not operate until the 50-year event. Ditch spills within the Grapevine Basin include uncontrolled left bank overtopping immediately west of 35th Avenue (approximately 115 cfs) from inflows due to the 100-year event, and controlled spills through the Northview Side Channel Weir for all return periods. Uncontrolled left bank overtopping appears to be prevalent through the 28th Avenue Basin from approximately 28th Avenue east to the Greeley No. 3 Ditch Wasteway (immediately east of 25th Avenue) from flows due to a 5-year storm and higher. Ditch spills in this area are significantly more critical due to extensive development both south and north of the ditch. The Clarkson Spill Structure diverts a majority of the flow from the Greeley No. 3 Ditch, especially during higher return periods (e.g., 50-year return period and greater). The results of the hydraulic unsteady flow modeling for the Existing Condition for all four basins and all five return periods are provided electronically on the CD included in Appendix B of this report.

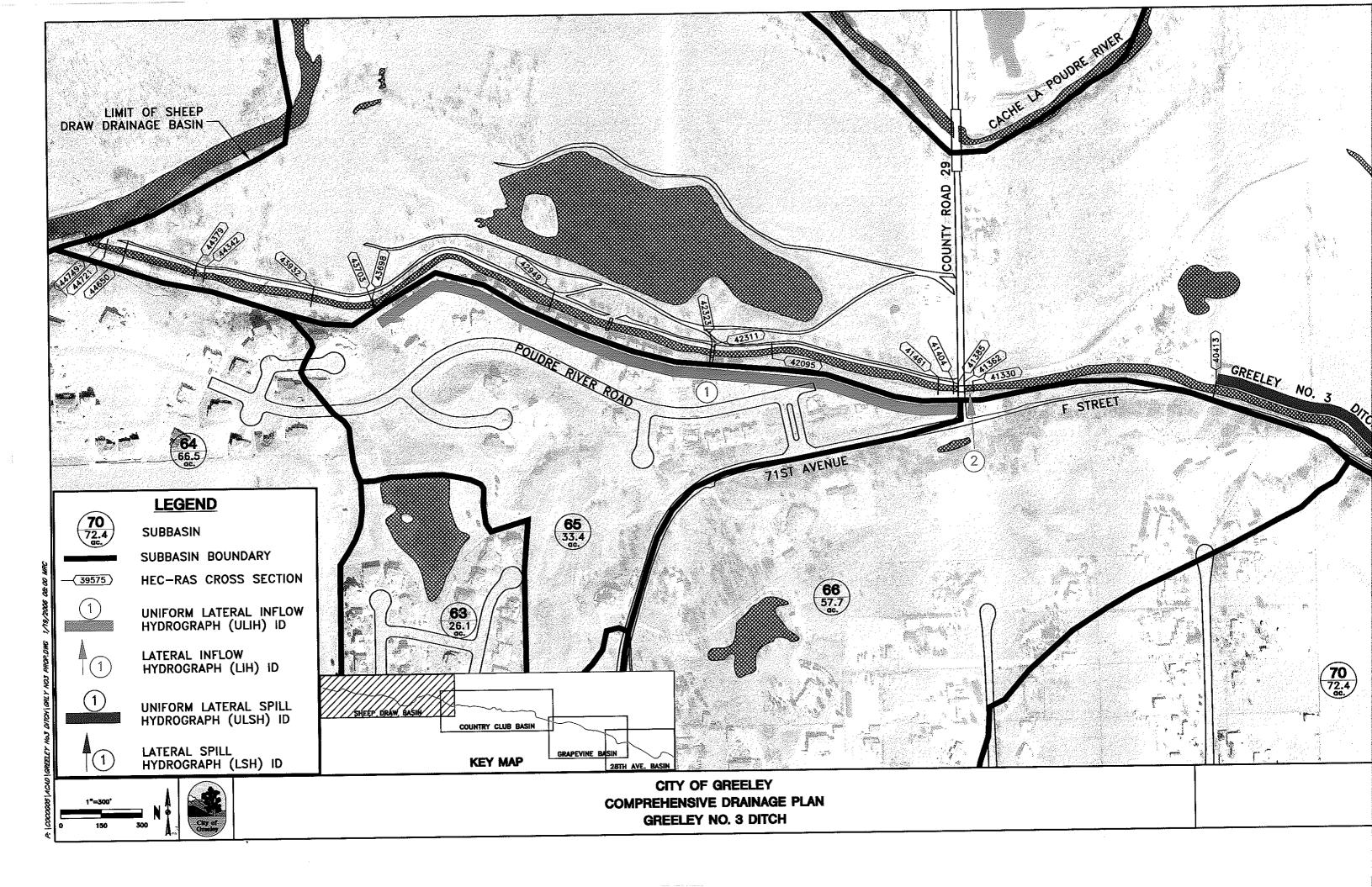
3.2.2 Hydraulic Modeling Results from the Proposed Condition Unsteady Flow Model

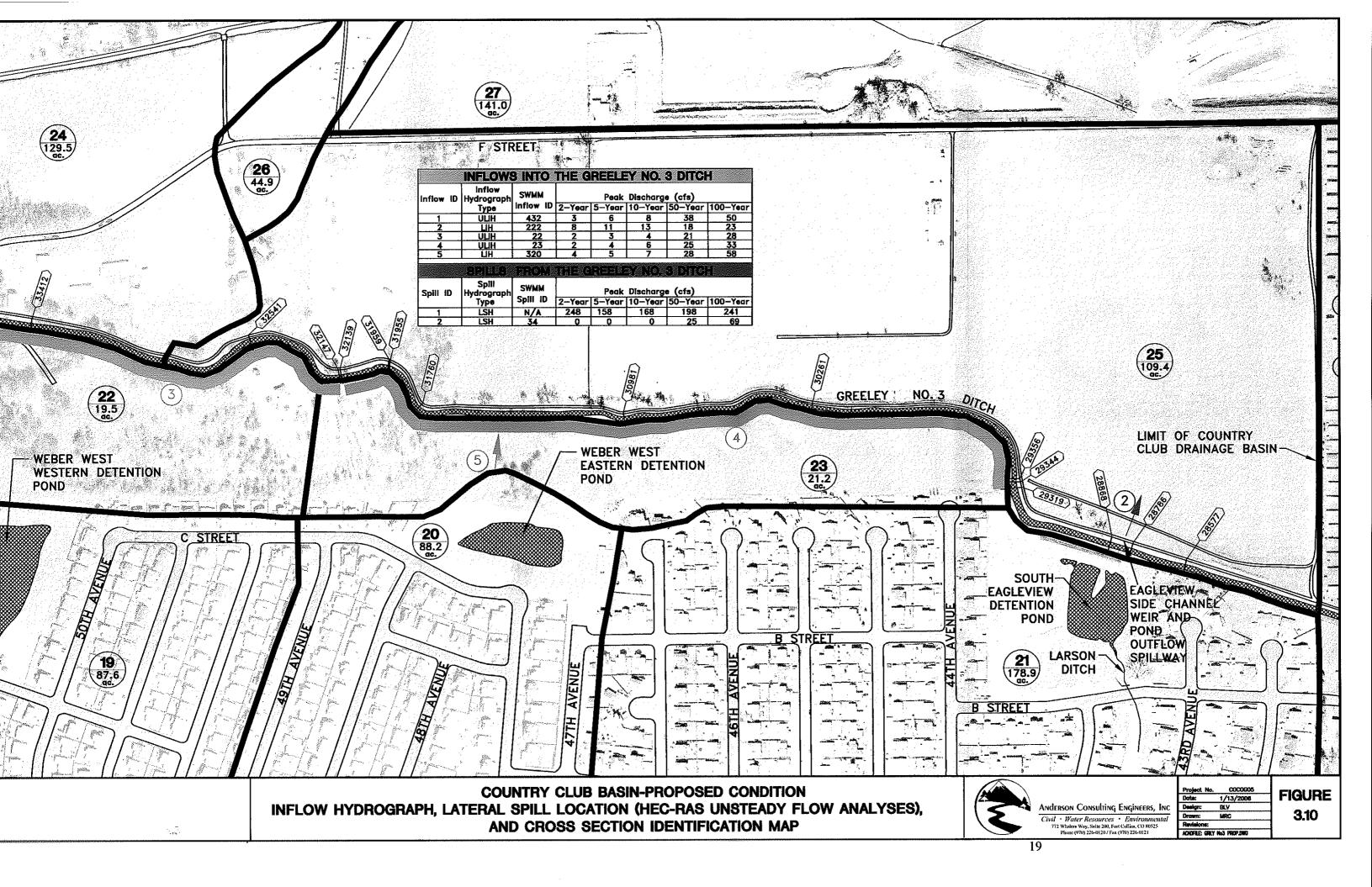
The construction of proposed improvements in the upper portions of the five major drainage basins generally decreases the flows contributing to the ditch, which in turn improves the overall effectiveness of the ditch in controlling bank overtopping. Figures 3.9 through 3.12 depict the Proposed Condition scenario for the four major basins.

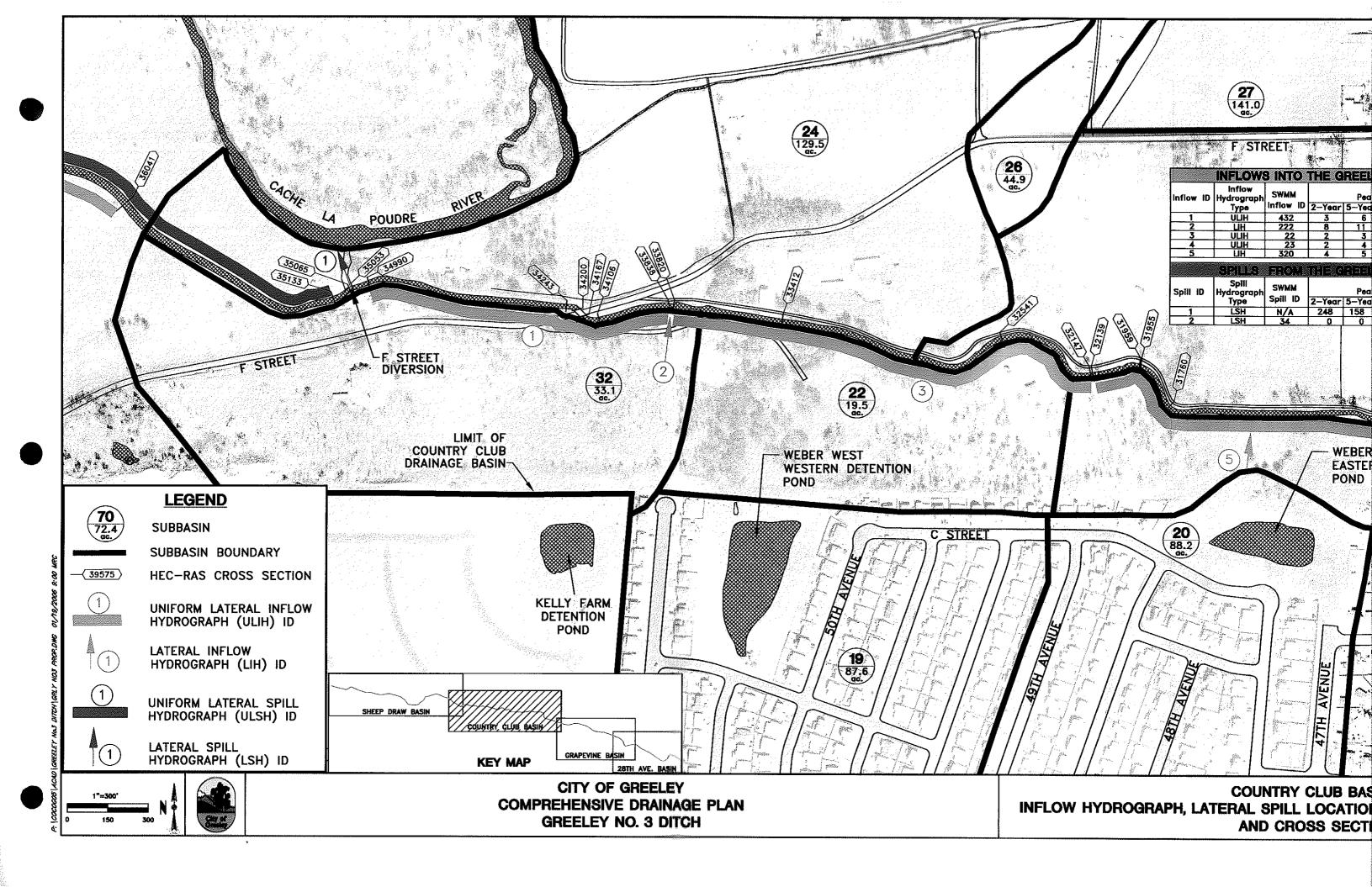
Proposed Condition spills generally remain the same as Existing Condition spills for a 10-year return period and larger within the limits of the Sheep Draw Basin. Ditch spills associated with the 2-year and 5-year return periods are higher due to elevated inflows into the ditch along the Sheep Draw drainageway. In the Country Club Basin, ditch spills will be slightly higher at the F Street Spill Structure (mainly due to generally higher inflows along Sheep Draw), but decrease at the Eagleview Side Channel Weir. The uncontrolled spill for the 100-year event upstream of 35th Avenue within the Grapevine Basin limits will be eliminated, with the spill at the Northview Side Channel Weir also significantly reduced. It should be noted that the future elimination of the uncontrolled spill and the reduction of the controlled spills at Eagleview and Northview can be attributed to the proposed removal of inflows into the ditch from Grapevine Subbasins 24 and 35 as well as flow along 35th Avenue (total of over 500 cfs), due to the Best-Way Park Regional Detention Pond. Uncontrolled left bank overtopping will persist within the 28th Avenue Basin, as Proposed Condition inflows will generally not be significantly reduced compared to the Existing Condition. The results from the hydraulic unsteady flow modeling for the Proposed Condition for all four basins and all five return periods are provided electronically in Appendix B.

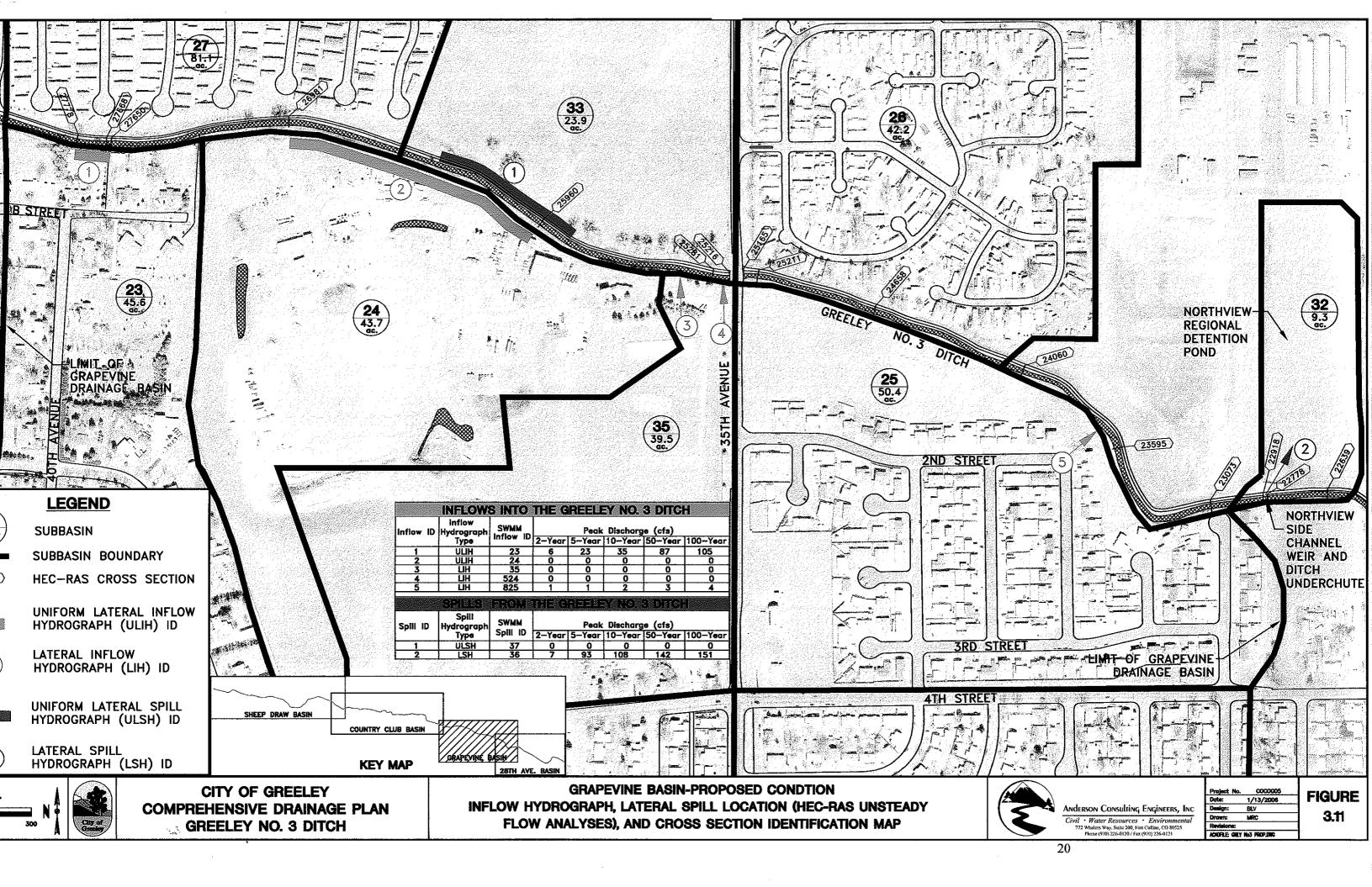


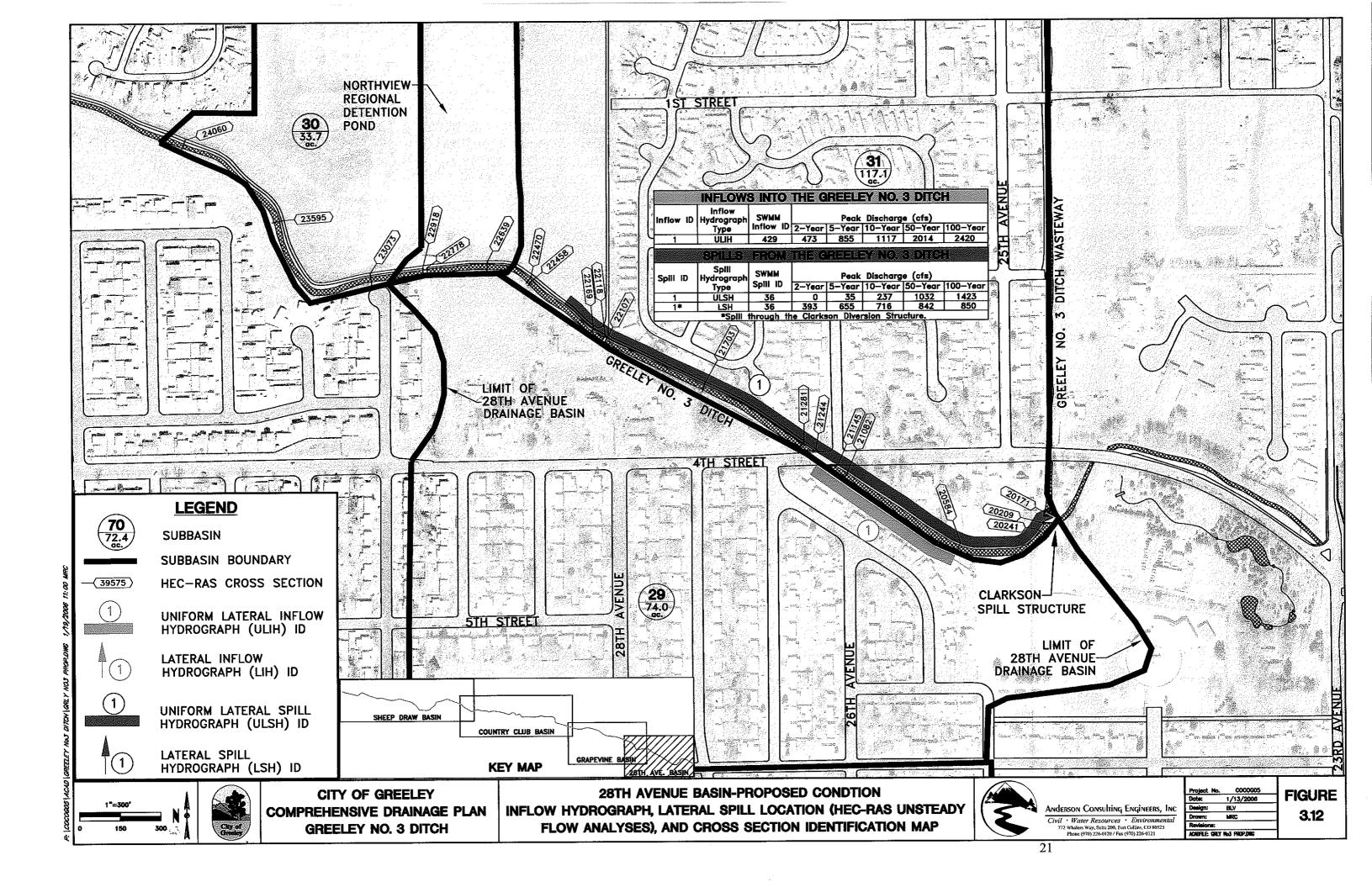












3.3 Summary

The Greeley No. 3 Ditch generally acts as an effective drainage boundary for all return periods under the Existing Condition through the limits of the Country Club and Grapevine Basins, with the exception of an uncontrolled spill for the 100-year event west of 35th Avenue in the Grapevine Basin. The ditch will become an even more effective drainage boundary during the Proposed Condition within the limits of these same two basins, with the elimination of the spill west of 35th Avenue during the 100-year event, along with the reduction of controlled spills at the Eagleview and Northview spill structures. Uncontrolled, left bank overtopping occurs during the Existing Condition generally for most return periods within the limits of the Sheep Draw and 28th Avenue Basins. This will continue to persist under the Proposed Condition in both basins, specifically in the 28th Avenue Basin due to the lack of space in that basin and along the ditch to implement drainage and flood control improvements.

22

APPENDIX A

DESIGN/REHABILITATION PLANS FOR SPILL STRUCTURES

APPENDIX A.1 F STREET SPILL STRUCTURE



LOVELAND

(25)

CALL UTILITY NOTIFICATION CENTER OF COLORADO -800-922-1987

CALL 2-BUSINESS DAYS IN ADVANCE BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND MEMBER UTILITIES.

GREELEY

34 (

WINDSOR

MCINITY MAP

F STREET

0

C

GREELEY NO. 3 "F" STREET DIVERSION GREELEY, COLORADO

27 SEPTEMBER 2002



PREPARED FOR:

THE CITY OF GREELEY

1001 9th AVENUE GREELEY, COLORADO 80631 (970) 336-4121 CONTACT: BERT LEAUTAUD, P.E.

PREPARED BY:



Drexel, Barrell & Co.

Engineers · Surveyors 4840 PEARL EAST CIRCLE, SUITE 114 BOULDER, COLORADO 80301 (303) 442-4338

CONTACT: CLIFF BROCKMAN, P.E.

пем	-	UNIT	QTY
DEMO EXISTING STRUCTURE	•	LS	1
STRUCTURAL FILL		TON	226
STRUCTURAL SONCRETE	~~~~	~~~~	70
RIP-RAP-(TYPE 'M')		ČY	40
TYPE II BEDDING		GY	15
CATWALKS		LF	26
STOPLOG ASSEMBLY		LF	28
FURNISH & INSTALL OVERSHOT GA	ATE.	LS	1
ELECTRICAL POWER W/METER		LS	1
BACKPILL AND COMPACTION (NON-	-STRUCTORAL)	TON.	<u>~</u> ₩
AQUATAPOXY COATING		SF	260

	SHEET INDEX				
SHEET NO.	SHEET DESCRIPTION]			
1	COVER SHEET	Į			
2	SITE PLAN/DEMOLITION PLAN]			
3	PROPOSED DIVERSION PLAN AND SECTIONS]			
4	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS]			
5	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS	Ì			

ALL WORK S	HALL BE CONSTRUCTED TO THE CITY OF GREELEY STANDAR	D SPECIFICATIONS.
APPROVED	CITY OF GREELEY DIRECTOR OF PUBLIC WORKS	DATE
APPROVED	CITY OF GREELEY DIRECTOR OF WATER & SEWER	DATE

PROJECT LOCATION MAP

THE GREELEY IRRIGATION COMPANY REVIEW & APPROVE FOR CONSTRUCTION

BENCHMARK

LOCATED IN A RANGE BOX AT THE INTERSECTION OF "F" STREET, AND 59th AVENUE. THIS MONUMENT IS THE NORTHEAST SECTION CORNER T5NR65WS04.

STRUCTURAL NOTES

1. GENERAL REQUIREMENTS:
A. ALL CONSTRUCTION SHALL COMPLY WITH THE 1997 UNIFORM BUILDING CODE, OR LATER EDITION ADOPTED BY THE GOVERNMENTAL JURISDICTION, AND ALL OTHER PERTINENT GOVERNMENTAL CODES, ORDINANCES AND REGULATIONS.

2. FOUNDATIONS: A. DESIGN IS BASED ON A MAT SLAB FOUNDATION, PLACED ON 2 FEET OF COMPACTED STRUCTURAL FILL MAXIMUM BEARING PRESSURE USED IN DESIGN = 1000

3. CONCRETE:
A. ALL CONCRETE SHALL COMPLY WITH THE LATEST EDITIONS OF THE ACI SPECIFICATIONS FOR STRUCTURAL CONCRETE, ACI 301, AND ACI BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE, ACI 318.

B. CONCRETE MIX DESIGN, AIR ENTRAINMENT, PLACEMENT, TRANSPORT, ETC. SHALL BE PER ACI SPECS. MIX DESIGN IS SUBJECT TO THE ENGINEER'S APPROVAL.
C. ALL CONCRETE SHALL BE MADE USING TYPE 1/1 CEMENT, WITH STONE AGGREGATE, AND SHALL DEVELOPE A MINIMUM 28—DAY COMPRESSIVE STRENGTH OF 3000 psi.
D. MIX DESIGN SHALL HAVE THE FOLLOWING PROPERTIES:

LAVABURD WATER COMMENT.

D. MIX DESIGN SHALL HAVE THE FOLLOWING PROPERTIES:

MAXMUM WATER/CEMENT RATIO:

SLUMP AT WALLS

4" TO 6"

SLUMP AT SLAGS

3" TO 5"

AIR ENTRANMENT

E. WATER ADDED TO CONCRETE AT THE SITE SHALL NOT EXCEED THE AMOUNT
PERMITTED BY THE BATCH TICKET. CONCRETE AT PLACEMENT TIME WHICH DOES NOT
MEET THE SPECIFIED SLUMP OR AIR CONTENT SHALL BE REFUSED BY THE CONTRACTOR.

F. ALL REINFORCING STEEL SHALL BE ASTM A615-GRADE 60, (INCLUDING #4 AND #5

PERMITTED BY THE BATCH TOKET. CONCRETE AT PLACEMENT TIME WHICH DOES NOT MEET THE SPECIFIED SUMAP OR AIR CONTENT SHALL BE REFUSED BY THE CONTRACTOR. F. ALL REINFORCING STEEL SHALL BE ASTM A615—GRADE 60, (INCLUDING #4 AND #5 BARS).

G. REINFORCING STEEL SHALL BE FABRICATED AND PLACED IN ACCORDANCE WITH THE ACI MANUAL OF STANDARD PRACTICE.

H. CONCRETE PROTECTION FOR REINFORCEMENT:

1) CONCRETE PLACED AGAINST EARTH: 3"

2) CONCRETE PLACED IN FORMS AND EXPOSED TO EARTH, WEATHER OR WATER (PRINCIPAL REINFORCEMENT): 2"

3) THE SHAD STRENPS: 1 1/2"

1. NO SPLICES OR WELDING OF REINFORCEMENT SHALL BE MADE EXCEPT AS DETAILED OR AUTHORIZED BY THE ENGINEER. LAP SPLICES, WHERE PERMITTED, SHALL BE 24"

MINIMUM UNLESS OTHERWISE NOTED.

J. DETAIL BARS IN ACCORDANCE WITH THE LATEST EDITIONS OF THE ACI DETAILING MANUAL AND ACI BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE. PROVIDE ALL ACCESSORIES NECESSARY TO SUPPORT REINFORCING AT THE POSITIONS SHOWN ON THE PLANS OR AS NOTED ABOVE.

K. SHOP DRAWINGS SHALL BE SUBMITTED FOR APPROVAL, IN REPRODUCIBLE FORM, OF ALL REINFORCING STEEL PRIOR TO FABRICATION.

1. PROVIDE 2—55 BARS WITH 2'—0" PROJECTION.

1. PROVIDE SFROM MAT SLABS TO WALLS AND COLUMNS SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS ON SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTING SHAD SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS AND SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS OF CONCRETE BARS TYPICAL FOR DUBBLE MAY WALL SHIPPORCING. ON NOT PLACE CORNER BARS FROM "INSIDE FACE TO INSIDE FACE". PROVIDE THREE CORNER BARS TYPICAL FOR DUBBLE MAY WALL SHIPPORCING. ON NOT PLACE CORNER BARS TYPICAL FOR

⚠

4. STEEL:
A. ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A36, UNLESS OTHERWISE
NOTED. STEEL PIPE SHALL CONFORM TO ASTM A53, GRADE B.
B. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN
ACCORDANCE WITH THE LATEST EDITIONS OF THE ASC MANUAL OF STEEL
CONSTRUCTION—ALLOWABLE STRESS DESIGN, AND AISC CODE OF STANDARD PRACTICE.

5. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL DIMENSIONS AND TO IMMEDIATELY NOTIFY THE ENGINEER OF ANY DISCREPANCIES, CONDITIONS NOT SHOWN OR THAT WHICH DIFFER FROM THOSE SHOWN ON THE DRAWINGS.

6. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING A SAFE WORKING ENVIRONMENT FOR ALL TRADES, AND FOR COMPLIANCE WITH ALL OSHA AND SAFETY RELATED



NOT VALID WITHOUT ORIGINAL SIGNATURE AND DATE

REVISION DESCRIPTIONS DATE ACREST GATE AND STOP LOG ASSY. 07 JAN 2003

5D 782 EW--1174 SHEET 1 OF 5

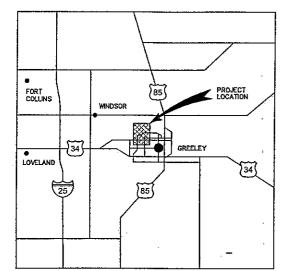


CALL UTILITY NOTIFICATION CENTER OF COLORADO -800-922-1987

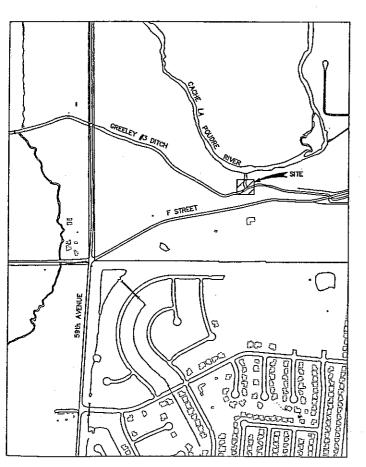
CALL 2-BUSINESS DAYS IN ADVANCE BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND

GREELEY NO. 3 "F" STREET DIVERSION GREELEY, COLORADO

27 SEPTEMBER 2002











PREPARED FOR:

THE CITY OF GREELEY

1001 9th AVENUE GREELEY, COLORADO 80631 (970) 336-4121 CONTACT: BERT LEAUTAUD

PREPARED BY:



Drexel, Bariell & Co. Engineers • Surveyors 4840 PEARL EAST CIRCLE, SUITE 114 BOULDER, COLORADO 80301 (303) 442-1338

CONTACH: CLIFF BROCKMAN, P.E.

ESTIMATES QUANTITIES				
ITEM	UNIT	QTY		
DEMO EXISTING STRUCTURE	LS	1		
STRUCTURAL FILL	TON	226		
STRUCTURAL CONCRETE	CY	70		
RIP-RAP (TYPE 'M')	CY	40		
TYPE II BEDDING	CY	15		
CATWALKS	LF	26		
STOPLOG ASSEMBLY	LF	28		
FURNISH & INSTALL HINGE CREST GATE	LS	1		
ELECTRICAL POWER/NEMA TYPE 4 ENCLOSURE (24"x30"x10") w/METER	LS	1		
BACKFILL AND COMPACTION (NON-STRUCTURAL)	TON	101		
AQUATAPOXY COATING	SF	260		

SHEET INDEX					
SHEET NO.	SHEET DESCRIPTION				
1	COVER SHEET				
2	SITE PLAN/DEMOLITION PLAN				
3	PROPOSED DIVERSION PLAN AND SECTIONS				
4	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS				
5	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS				

ALL WORK SI	HALL BE CONSTRUC	TED TO THE CITY OF GREELE	Y STANDARD SPECIFIC	CATIONS.
APPROVED	Mellin City of GREEK	U Stub	u 9/1.	30/0Z
APPROVED	CITY OF GREEK	DIRECTOR OF WATER 12 SE		/25/02

BENCHMARK

LOCATED IN A RANGE BOX AT THE INTERSECTION OF "F" STREET, AND 58th AVENUE. THIS MONUMENT IS THE NORTHEAST SECTION CORNER TSURGESUSO4.

STRUCTURAL NOTES

- 1. GENERAL REQUIREMENTS:
 A. ALL CONSTRUCTION SHALL COMPLY WITH THE 1997 UNIFORM BUILDING CODE, OR LATER EDITION ADOPTED BY THE GOVERNMENTAL JURISDICTION, AND ALL OTHER PERTINENT GOVERNMENTAL CODES, ORDINANCES AND REGULATIONS.
- 2. FOUNDATIONS: A. DESIGN IS BASED ON A MAT SLAB FOUNDATION, PLACED ON 2 FEET OF COMPACTED STRUCTURAL FILL. MAXIMUM BEARING PRESSURE USED IN DESIGN = 1000

- 3. CONCRETE:

 A. ALL CONCRETE SHALL COMPLY WITH THE LATEST EDITIONS OF THE ACI SPECIFICATIONS FOR STRUCTURAL CONCRETE, ACI 310, AND ACI BUILDING CODE RECORDERIENTS FOR REINFORCED CONCRETE, ACI 310.

 B. CONCRETE MIX DESIGN, ARE ENTRAINMENT, PLACEMENT, TRANSPORT, ETC. SHALL BE PER ACI SPECS. MIX DESIGN IS SUBJECT TO THE ENGINEER'S APPROVAL.

 C. ALL CONCRETE SHALL BE MADE USING TYPE I/I CEMENT, WITH STONE AGGREGATE, AND SHALL DEVELOPE A MINIMUM 22-DAY COMPRESSIVE STRENGTH OF 3000 pal.

 D. MIX DESIGN SHALL HAVE THE FOLLOWING PROPERTIES:

 MAXIMUM WATER/CEMENT RATIO:

 O.51

 4" TO 6"
- D. MIX DESIGN SHALL HAVE THE FOLLOWING PROPERTIES:
 MAXIMUM WATER/CEMENT RATIO:
 0.51
 SLUMP AT WALLS
 4" TO 5"
 SILMP AT SLABS
 3" TO 5"
 AIR ENTRAINMENT
 5% TO 7%
 E. WATER ADDED TO CONCRETE AT THE SITE SHALL NOT EXCEED THE AMOUNT
 PERMITTED BY THE BATCH TICKET. CONCRETE AT PLACEMENT THE WHICH DOES NOT
 MEET THE SPECIFIED SLUMP OR AIR CONTENT SHALL BE REFUSED BY THE CONTRACTOR.
 F. ALL REINFORCING STEEL SHALL BE ASTM A615-GRADE 60, (INCLUDING #4 AND #5

- PERMITTED BY THE BATCH TICKET. CONCRETE AT PLACEMENT I LIBE. WHICH DUSTS NOT MEET THE SPECIFIED SUMP OR AIR CONTENT SHALL BE REFUSED BY THE CONTRACTOR. F. ALL REINFORCING STEEL SHALL BE ASTM A615—GRADE 60, (INCLUDING #4 AND #5 BARS).

 G. IREINFORCING STEEL SHALL BE ASTM A615—GRADE 60, (INCLUDING #4 AND #5 BARS).

 G. IREINFORCING STEEL SHALL BE ASTM A615—GRADE 60, (INCLUDING #4 AND #5 BARS).

 G. IREINFORCING STEEL SHALL BE ASTM A615—GRADE 60, (INCLUDING #4 AND #5 BARS).

 H. CONCRETE PROTECTION FOR REINFORCEMENT:

 1) CONCRETE PLACED IN FORMS AND EXPOSED TO EARTH, WEATHER OR WATER (PRINCIPAL REINFORCEMENT):

 2) CONCRETE PLACED IN FORMS AND EXPOSED TO EARTH, WEATHER OR WATER (PRINCIPAL REINFORCEMENT):

 1) SES AND STRENGED:

 1 1/2"

 1 NO SPUICES OR WELDING OF REINFORCEMENT SHALL BE MADE EXCEPT AS DETAILED OR AUTHORIZED BY THE ENCINEER. LAP SPLICES, WHERE PERMITTED, SHALL BE 24" MINIMUM UNLESS OTHERWISE NOTED.

 J. DETAIL BARS IN ACCORDANCE WITH THE LATEST EDITIONS OF THE ACI DETAILING MANUAL AND ACI BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE. PROVUDE ALL ACCESSORIES NECESSARY TO SUPPORT REINFORCING AT THE POSTIONS SHOWN ON THE PLANS OR AS NOTED ABOVE.

 K. SHOP DRAWNINGS SHALL BE SUBMITTED FOR APPROVAL, IN REPRODUCIBLE FORM, OF ALL REINFORCING STEEL PRIOR TO FABRICATION.

 L. PROVIDE 2-#5 BARS WITH 2'-O" PROJECTION AROUND ALL OPENINGS IN CONCRETE. IN DIRECTOR OF APPROVAL BE IN PLACE WHEN THE REINFORCING BAR INSPECTION FOR THE FOOTINGS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE IN THE FOOTINGS SHALL BE INSTALLED PRIOR TO PLACEMENT OF CONCRETE IN THE FOOTINGS SHALL BE IN PLACE WHEN THE REINFORCING BAR INSPECTION FOR THE FOOTINGS TAKES PLACE.

 N. PROVIDE CONNER BARS AT ALL WALL INTERSECTIONS. SIZE AND SPACING OF BARS SHALL MATCH HORIZONTAL WALL REINFORCING. DO NOT PLACE CORNER BARS FROM "INSIDE FACE". PROVIDE THREE CONNER BARS TYPICAL FOR PROVIDED BY THE ENGINEER.

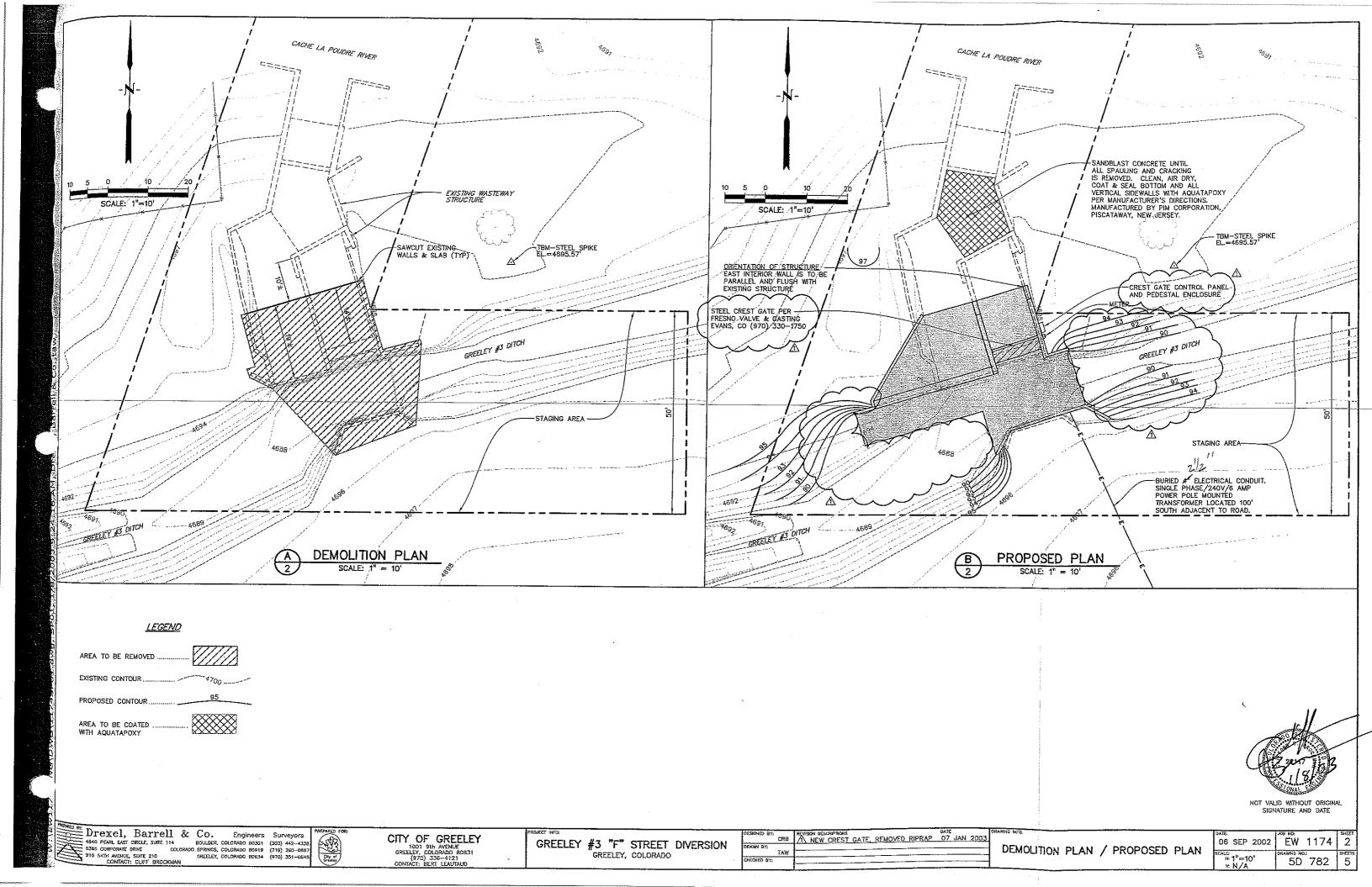
 P. CONTRACTOR SHALL PROVIDE PROTECTION AND INSULATION OF CONCRETE AGAINST AND HORIZONTAL KEYS, UNLESS OTHERWISE SHOWN. ALL CONSTRUCTION JOINTS S
- 4. STEEL:
 A. ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A36, UNLESS OTHERWISE
 NOTED. STEEL PIPE SHALL CONFORM TO ASTM A53, GRADE B.
 B. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN
 ACCORDANCE WITH THE LATEST EDITIONS OF THE AISC MANUAL OF STEEL
 CONSTRUCTION—ALLOWABLE STRESS DESIGN, AND AISC CODE OF STANDARD PRACTICE.
- 5. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL DIMENSIONS AND TO IMMEDIATELY NOTIFY THE ENGINEER OF ANY DISCREPANCIES, CONDITIONS NOT SHOWN OR THAT WHICH DIFFER FROM THOSE SHOWN ON THE DRAWINGS.
- THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING A SAFE WORKING ENVIRONMENT FOR ALL TRADES, AND FOR COMPLIANCE WITH ALL OSHA AND SAFETY RELATED REGILATIONS.

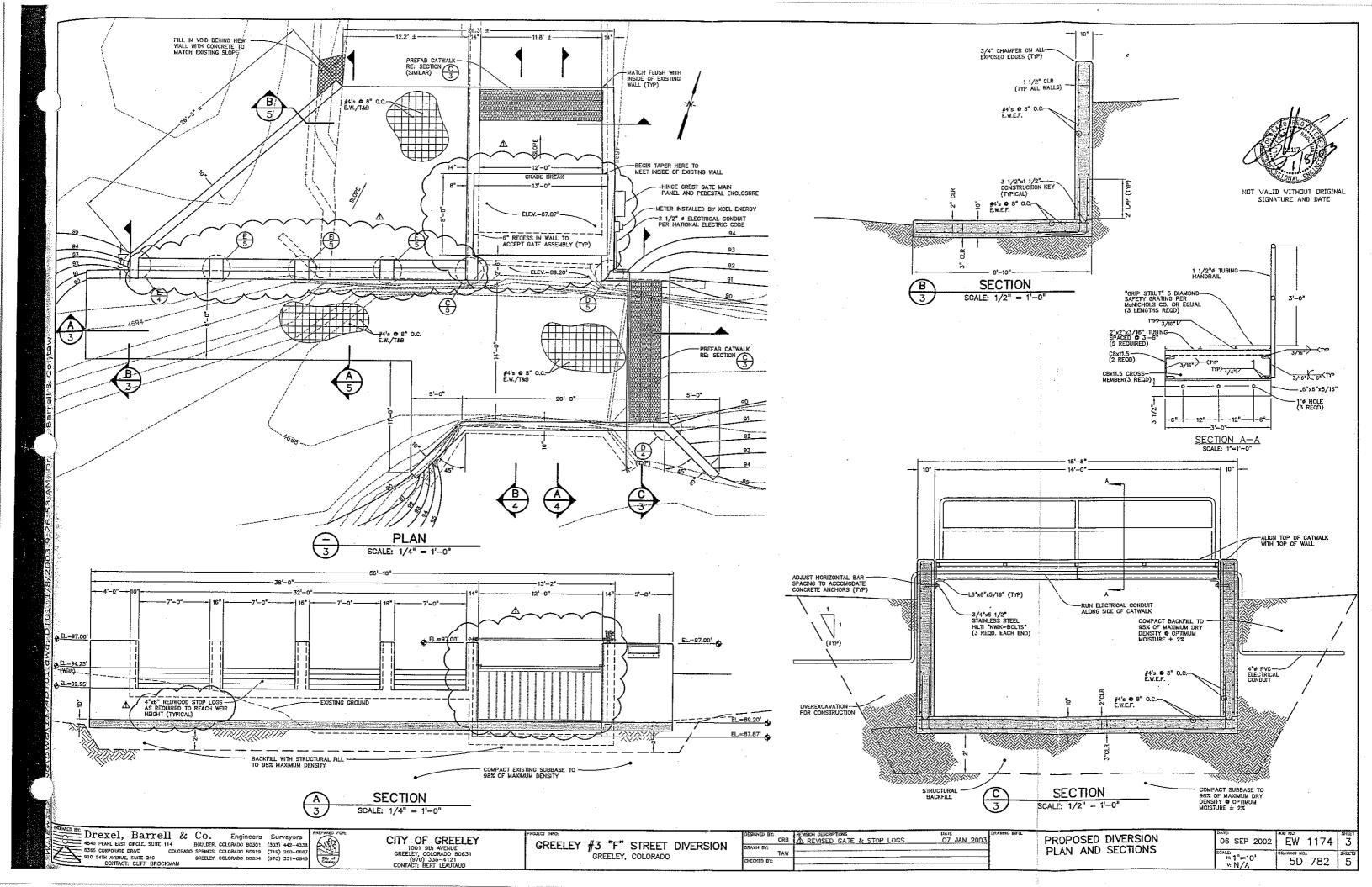


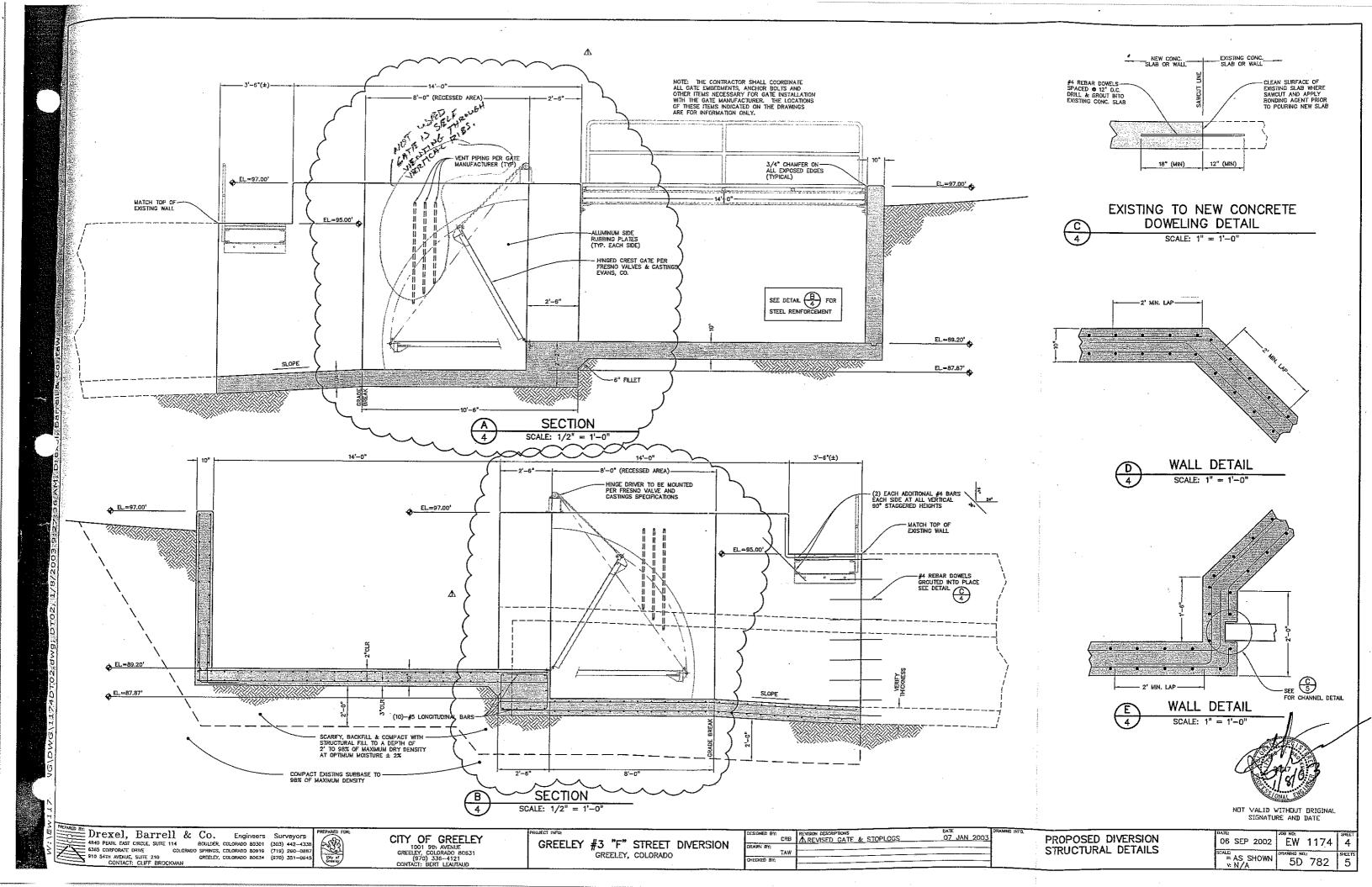
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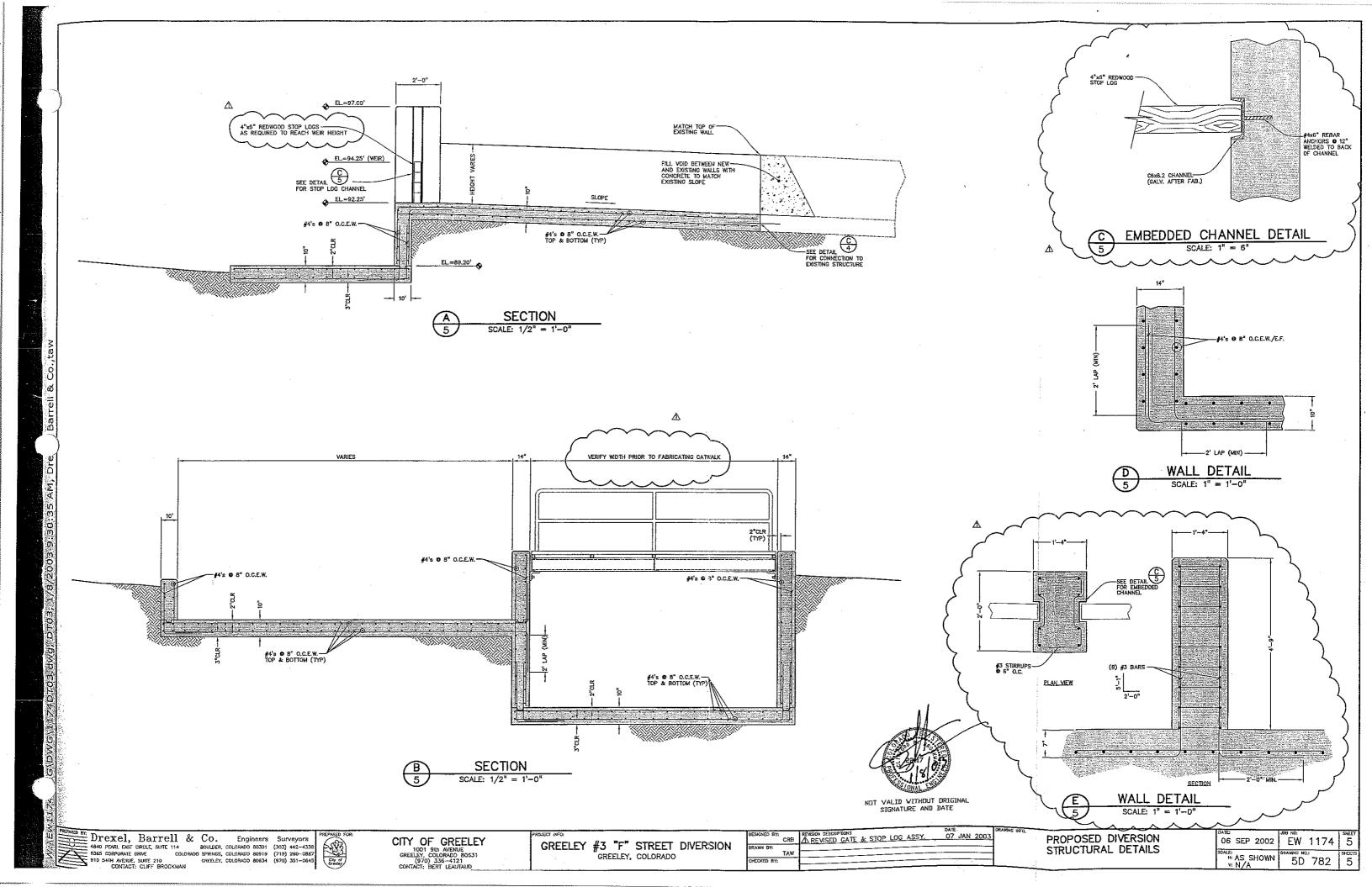
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REVISION DES





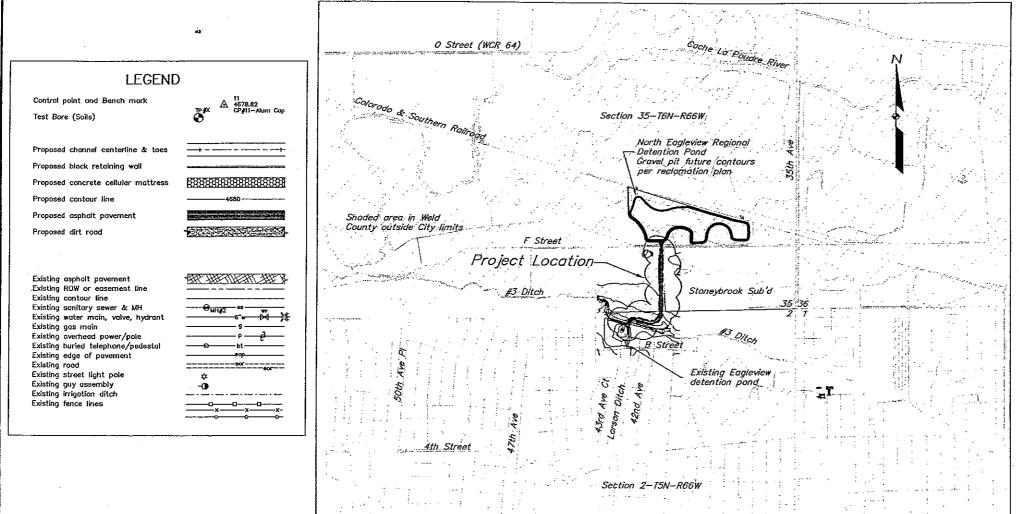




APPENDIX A.2 EAGLEVIEW SIDE CHANNEL WEIR

NORTH EAGLEVIEW DRAINAGE CHANNEL CITY OF GREELEY, CO

July, 2003



Construction of structures within #3 Ditch as shown in these plans

is approved by the Board of Directors of the Greeley Irrigation Co.

President

Secretary

SHEET INDEX

PROJECT DVERVIEW, GENERAL NOTES ALIGNMENTS, SOILS, CONTROLS, SEVERS CHANNEL PLAN & PROFILE 0-15 TO 8+00 CHANNEL PLAN & PROFILE 8+00 TO 16+00 CHANNEL PLAN & PROFILE 16+00 TO 24+03 SHEET SHEET SHEET IMPROVEMENTS - EAGLEVIEW POND, #3 DITCH SHEET CHANNEL WALLS LAYDUT POND & #3 SPILL PROFILES 21+00 TD 24+12 10 #3 BOX CULVERT LAYOUT & BAR SCHED
11 #3 BOX CULVERT DETAILS & DIMENSIONS SHEET SHEET 12 F ST BOX CULVERT LAYOUT & BAR SCHED SHEET SHEET 13 F ST BOX CULVERT DETAILS & DIMENSIONS 14 WINGWALLS 15 TYP SECS: DROP STRUCTURE, CHANNEL, WALLS
16 DITCH ROAD PLAN & PROFILE 0+00 TO 8+00
17 DITCH ROAD, IRRIGATION DITCH PROFILE SHEET SHEET SHEET 18 TRAFFIC CONTROL PLAN SHEET 19 CRUSS SECTIONS 0+50 TO 3+50 20 CROSS SECTIONS 4+00 TD 8+50 SHEET 21 CROSS SECTIONS 9+00 TO 13+00 13+73 TI 16+50 SHEET 22 CROSS SECTIONS 23 CROSS SECTIONS 17+00 TO 19+50 24 CRUSS SECTIONS 20+00 TO 22+25

SHEET 26 CROSS SECTIONS 23+51 TO 24+03, VOLUMES

22+50 TO 23+15

LOCATION, LEGEND, INDEX

LOCATION MAP

1" = 1,000' (24"x36') 1" = 2,000' (11"x17")



Construction must be in accordance with applicable City of Greeley construction standards. The City's acceptance allows for plan distribution and permit application. The City's acceptance shall not relieve the design engineer's responsibility for errors, omissions, or design deficiencies for which the City is held harmless.

25 CRUSS SECTIONS

	Approved:	Date:
]	Director of Water & Sewer	
-	Approved:	Date:
	Director of Public Works	

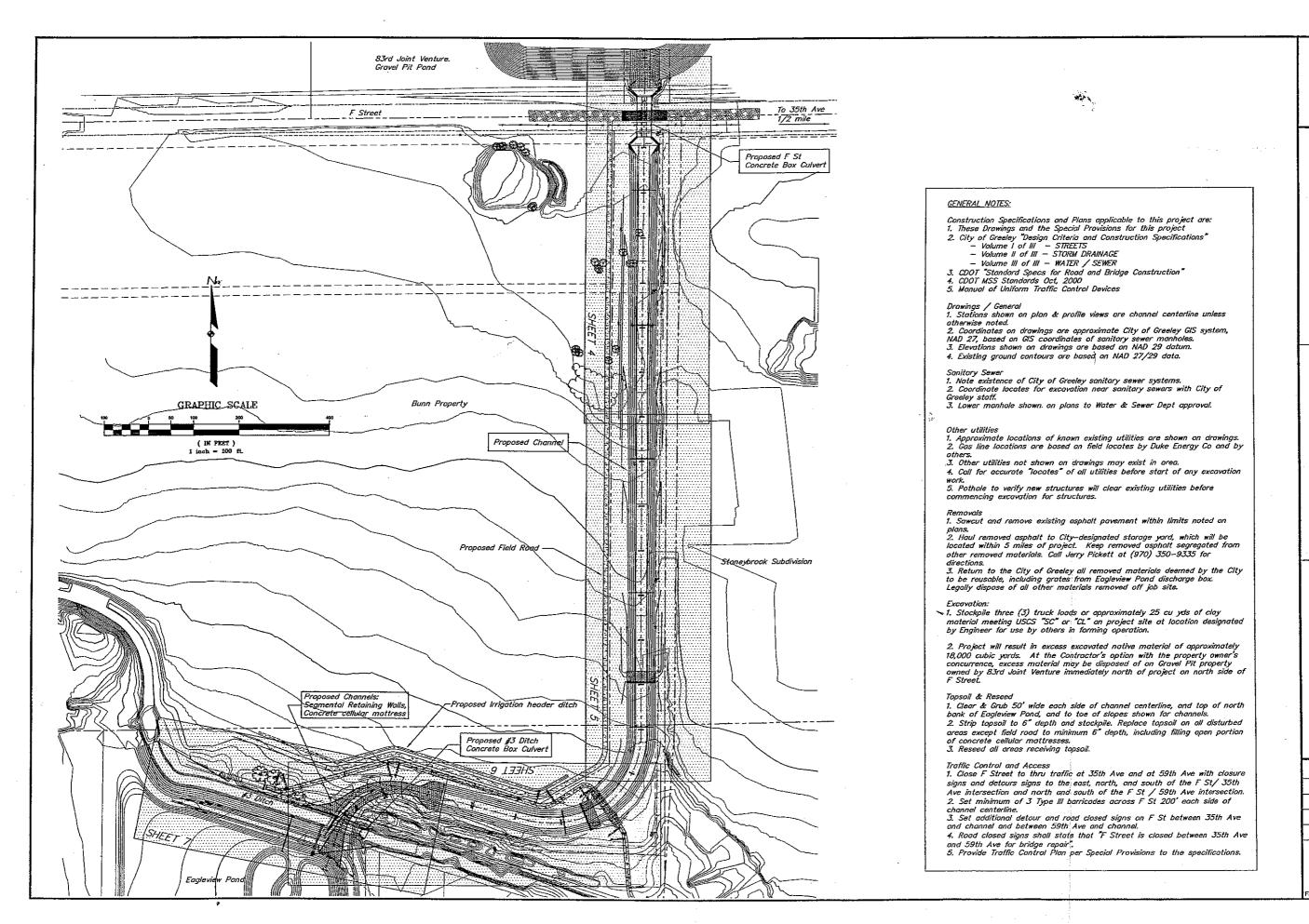
CITY OF GREELEY, CO
condrey, colo
80434
DRAINAGE CHANNEL

LOCATION, LEGEND,

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	Drawn By WN
	Checked By TEB
ē.	Date 7/16/03
	Scale as noted
	Job No. 02.08
	SHEET #
	1

File gevPlan.dwg



PROJECT OVERVIEW GENERAL NOTES

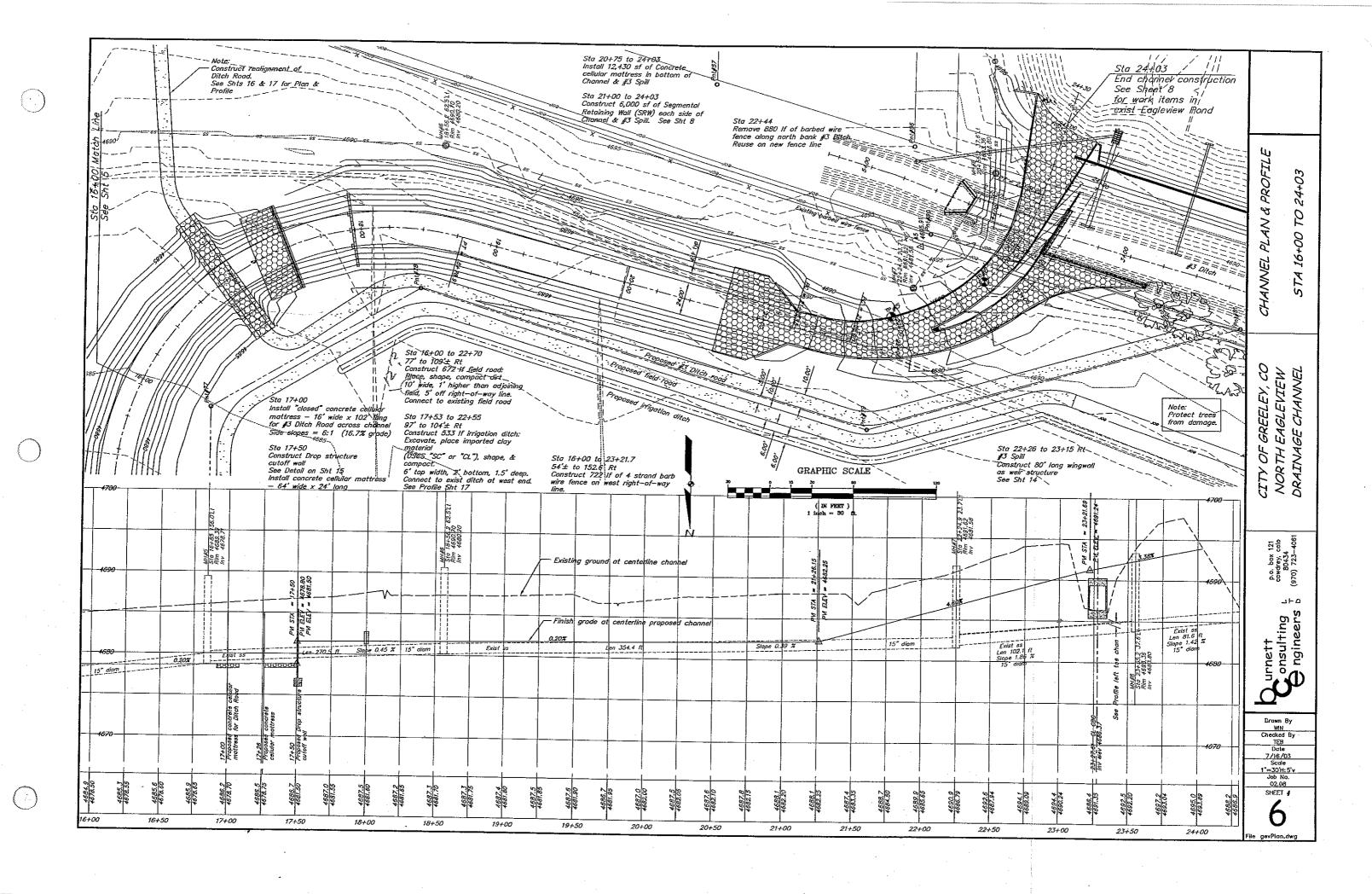
CITY OF GREELEY, CO NORTH EAGLEVIEW DRAINAGE CHANNEL

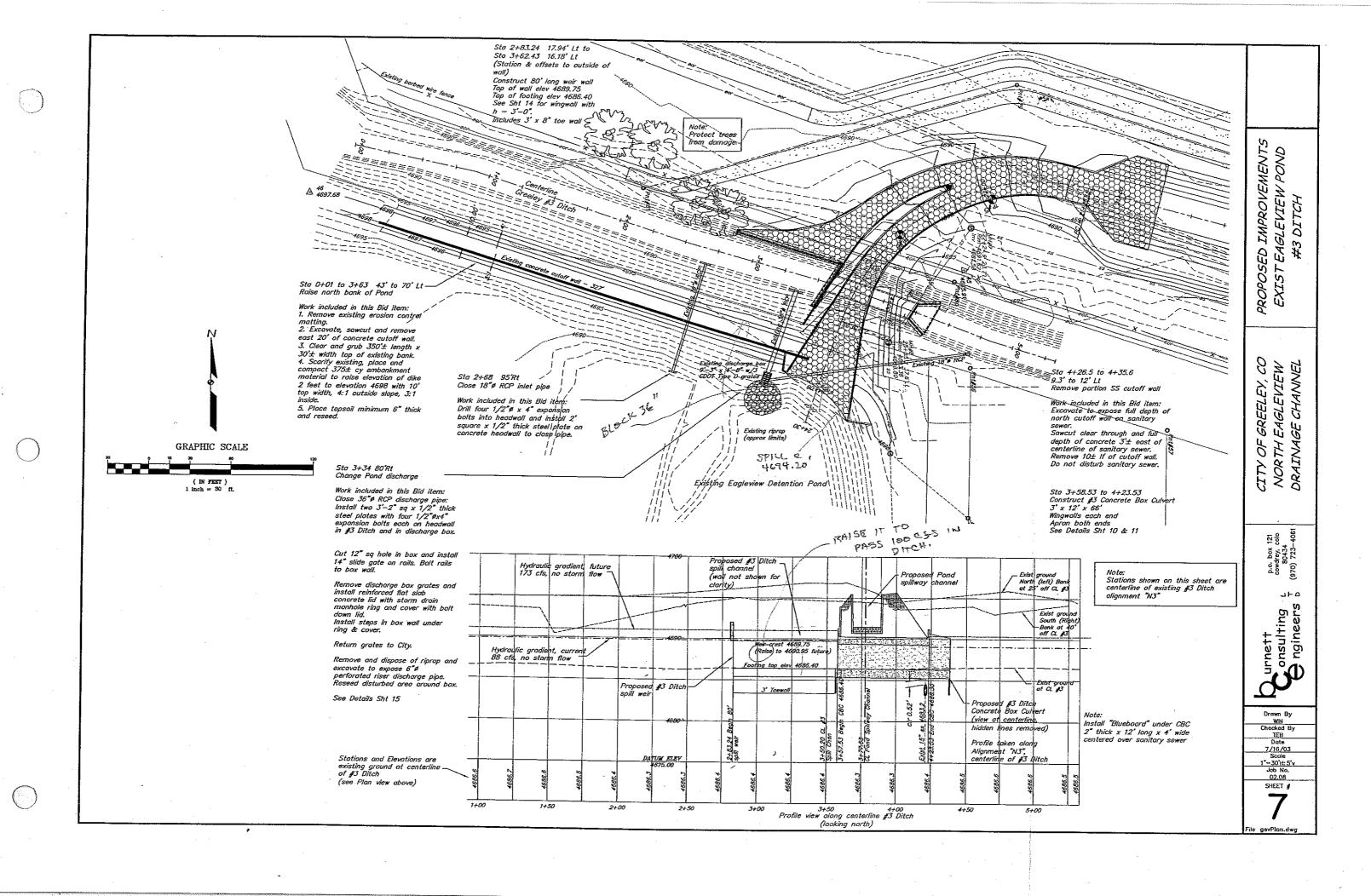
> p.o. box 121 cowdrey, colo 80434 (970) 723-4061

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Checked By
TEB
Date
7/16/03
Scale
1*=100'
30 No.
02.08
SHEET #

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#3 Ditch Concrete Box Culvert:

Conform to CDOT M Standard M-601-1 for CBC Conform to CDOT M Standard M-601-20 for wingwalls

Design: Flow max = 195 cfs Depth, up = 4.5 ft

Dimensions:

Since S_{t} S_{t} Wall thickness, Tw = 10"

Wingwall height & angles: (see table on Wingwalls Details Sht)

Invert elev at upstream end = 4686.40 Invert elev at downstream end = 4586.30 Invert elev at CL channel = 4686.37 Slope = 0.154%

Sto 23+27.61 finish channel elev = 4691.44 Top of top slab at centerline channel = 4690.25

Construct concrete apron each end of CBC

Use 12' span x 6' rise by 10.5" top slab thickness for all steel sizes per sheet 2 of M-601-1.

SINGLE CONCRETE BOX CULVERT DIMENSIONS & QUANTITIES (EXCLUDING HEADWALLS & TOEWALLS)

	80	X SIZE		FILL	S	AB &	: WALL		BAR SIZES		Ι.,	DIMENSIONS					QUANTITIES				
S	R	HT.	WIDTH	HEIGHT ALLOWED		(NESS	(INCHES)	t1*&b1	t ₂	b ₂	w₁* & w2	C1*	C ₂	dı♣	h ₁	h ₂	V	V2	V3		
FT.	FT.	FTIN.	FTIN.	FTFT.	Τt	Ть	TW	#	#	#	. #	#	#	NO.	FTIN.		FTIN.			CONCRETE CU.YDS./LIN.FT	REBAR STL
Ì	ļ		بلآجال	21274.70	אַבּנוּ	17.5	11.5	4	7	.7.	j	5	5		3-8	3-4	11-1	3-4	3-4	1.905	328
	$\overline{\zeta}$	7-11	13-8	0 TO 8	10.5	12.5	10	4	1 /		4		5	┝~	3-11	3-8	6-8	3-4	2-6	محتود	-
1	6)	3	13≃8^ 13~8	<u>>810-12</u> ~			~~0~~	~~*~~			man	بقيا	1.5	_60 __	- 19معر	~ <u>z-9</u>	ક≍ મ⊷	ميميد	رقيق	1.341	306)
1	كرأ	9-3.5		>16 TO 20	15.5	18 20.5	10	4 4	8	8	4	5	5	[3-6	2-9	7-1	3-5	3-0	1.783	319
}	7	9-11	13-8	0 TO 8	10.5	12.5	10	4	7	_7	5	6	5		4-1	3-9	7-5 8-8	3-7	3-2 2-11	2.037 1.464	341 351
(12)	8	10-4		>8 TO 12	15.5	15 18	10	4	8 8	8	4	6	5	68	3-4	2-9	8-11	36	2-9	1,675	358
	Ĺ	11-3.5			18.5	21	10	4	8	8	4	5	5		3-6	2-10 3-0	9-1	3-5	3-0	1.907	338

HEADWALL AND TOEWALL QUANTITIES

HEADWALL SKEW ANGLE					74% 1	0 60%	59% TO 45%			
SPAN - S	Z	STIRRUPS	REBAR QUANT.	Z	STIRRUPS	REBAR QUANT.	₹	STIRRUPS	REBAR QUANT.	
	#	#	LBS./LIN.FT.	#	#	LBS./LIN.FT.	#	#	LBS./LIN.FT.	
6	4	4	22.1	4	4	21.9	4	4	21.3	
8	4	4	22.5	4	4	22.3	5	4	28.0	
10	.5.	4	28.2	5	4	27.9	7	-4	43.2	
[12]	5	4	27.6)6	4	34.5	8	5	56.4	
14	~€	4	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	7	4	41.9	10	5	81,5	
16	6	4	32.3	8	5	53,3	*	*	*	
18	7	4	39.0	9	5	62.6	*	*	*	
20	7	4	38.6	11	6	96.9	*	*	*	
CONCRE	ĪΕ	QUANTITY	= 0.085 (Y.U	DS./LIN.FT		-			

NOTES: QUANTITIES ARE PER LINEAR FOOT (OF HEADWALL) FOR ONE HEADWALL AND TOEWALL AND INCLUDE ALL HEADWALL AND TOEWALL REINFORCING STEEL.

* A SKEWED HEADWALL IS NOT RECOMMENDED FOR THESE SPANS. A SPECIAL DESIGN IS REQUIRED.

FOR HEADWALL AND TOCKMALL DETAILS SEE PREMIOUS SHEET.

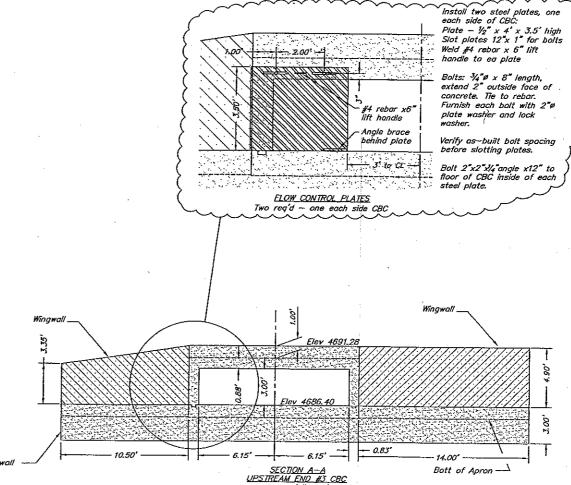
WHEN THE HOMINAL FILL HEIGHT FOR THE CONCRETE BOX CULVERT IS $\leq 2'-0$ °, all reinforcing stell in the headwall shall be epoxy-coated, also, those reinforcing bars designated by an asterisk (**) and the d_1 bars in the top mat of the top slab shall be epoxy-coated.

REINFORCING QUANTITIES INCLUDE BOTH EPOXY-COATED AND UNCOATED BARS.

WHEN AN R (RISE) OF LESS THAN SIX FEET IS REQUIRED, USE THE BAR SIZES AND THE SLAB AND WALL THICKNESSES FOR THE SIX FOOT RISE (IF AVAILABLE).

▲ THE SIZE OF d 1 BARS IS #4. THE NUMBER OF BARS REQUIRED IS LISTED.

Tables taken from CDOT M Standard M-601-1, sheet 2 Use bar sizes and dimensions for 12' span x 6' rise as shown.



Scale: 14" = 1"

CITY OF GREELEY, CO NORTH EAGLEVIEW DRAINAGE CHANNEL

E BOX CULVERT & BAR SCHED

#3 DITCH

٦٢Δ urnett onsulting ngineers

TEB Date 7/16/03 Scale as noted Job No. 02.08 SHEET #

APPENDIX A.3 NORTHVIEW SIDE CHANNEL WEIR

539-3291 GLEW Ceil

10:00 THUPS 01/24/02 BOTTA OT CBC

ENG @ DREVEL BARRELL CLIFF BLOCKMAN *(303) 442-4338

UNIT

QUANTITY

UNIT

BASE BID

LIST OF APPROXIMATE QUANTITIES

DETENTION POND HEADWALL W/ TRASHRACL & CONC. PAD 24" RCP CLASS III Pipe Stub & Plug @ MH "E"

BID ALTERNATE NO. 1

LIST OF APPROXIMATE QUANTITIES

17 4'Ø INSIDE DROP MANHOLE PER GREELEY STD. DWG. X19

6" GEOLINK CONCRETE INTERLOCKING BLOCKS*

4" GEOLINK CONCRETE INTERLOCKING BLOCKS RIPRAP (TYPE M)

I-11 CONCRETE WEIR WALL & South pur of Ellute
I-12 EMERGENCY SPILLWAY CUTOFF WALL 7.1 co P.
I-13 4" CONCRETE CHUTE PAVING

DITCH CONTROL STRUCTURE W/ CATWALK

1-26 SHORE EXISTING TIMBER WALL FOR UNDERCHUTE CONSTRUCTION
1-27 REMOVE CONCRETE TRICKLE CHANNEL

CATWALK GUARDRAILS
CHUTE SIDEWALL GUARDRAILS
NORTH CULVERT HEADWALL GUARDRAIL
SOUTH CULVERT HEADWALL GUARDRAIL
SEEDING (NATIVE)

REMOVE AND SALVAGE EXISTING RIPRAP

1-14 CHUTE SIDEWALLS
1-15 16'x3' BOX CULVERT W/ PARAPET WALLS
1-16 NORTH CONCRETE HEADWALLS
1-17 DITCH SIDE WEIR WALL

REMOVE AND REPLACE ASPHALT
REMOVE AND REPLACE BASE COURSE DRIVE
STRAW BALE INLET PROTECTION

5' DIAMETER CONCRETE MANHOLE
30" RCP, CLASS III (COMPLETE IN PLACE)
30" RCP F.E.S. (COMPLETE IN PLACE)
LOWER 16" DUCTILE IRON WATER MAIN

RIPRAP (TYPE 'M')
TYPE II BEDDING MATERIAL

8" PVC SANITARY SEWER

UNCLASSIFIED EXCAVATION UNCLASSIFIED EMBANKMENT

TYPE II BEDDING MATERIAL

MIRAFI 140N FABRIC

6" CONCRETE BIKEPATH

DITCH CLAY LINER

STRAW BALE INLET PROTECTION

SEEDING (NATIVE)

ITEM DESCRIPTION

EXPORT OFFSITE
SILT FENCE

ITEM ITEM DESCRIPTION

Coverete

EX 126

HERMAN HEL 539-45-99

FINAL CONSTRUCTION PLANS

NORTHVIEW REGIONAL DETENTION POND, OUTFALL SYSTEM AND THE GREELEY NO. 3 DITCH UNDERCHUTE

A PART OF THE NORTHWEST 1/4, OF SECTION 1, TOWNSHIP 5 NORTH, RANGE 66 WEST, OF THE 6TH P.M. CITY OF GREELEY, COUNTY OF WELD, STATE OF COLORADO



CALL UTILITY NOTIFICATION CENTER OF COLORADO BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND

BENCHMARK #66635A - A 2-1/2" ALUMINUM CAP IN BOX-100'# WEST OF 35TH AND 150'± NORTH OF 'F' STREET AT SOUTHERLY R.O.W. OF RAILROAD. Coche C EL.=4671.23 1929 DATUM

DETENTION POND

VICINITY MAP

NOT TO SCALE

Clover Creek —Subdivision

30" Outfall Pipe

4th Street

'C' Street

w Community

Land Lease

Existing
Outfall structure to
Greeley #3 Wasteway

5th Street

9th Street

CONTRACT DOCUMENTS ISSUED JUNE 12, 2001

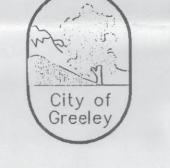
	SHEET INDEX
SHEET NO.	SHEET DESCRIPTION
1	COVER SHEET
2	HORIZONTAL CONTROL PLAN
3	DETENTION POND GRADING AND CONTROL PLAN
4	DETENTION POND DETAILS
5	BOX CULVERT UNDERCHUTE
6	DETENTION POND OUTFALL PLAN & PROFILE (1 OF 2)
7	DETENTION POND OUTFALL PLAN & PROFILE (2 OF 2
8	DITCH UNDERCHUTE DETAILS
9	DITCH CONTROL STRUCTURE
10	DITCH SIDEWEIR DETAILS
- 11	CDOT M-601-20
12	MODIFIED CDOT M-601-1-1
13	PIPELINE DETAILS

PREPARED FOR:

City of Greeley Public Works

1000 10TH STREET GREELEY, CO 80631 (970) 336-4031

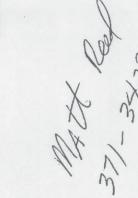
CONTACT: RON HOAGLAND, P.E.



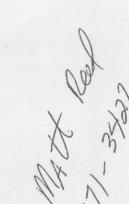
PREPARED BY:

Drexel Barrell & Co. Engineers • Surveyors 4840 PEARL EAST CIRCLE, SUITE 114 BOULDER, COLORADO 80301

> CONTACT: CLIFFORD BROCKMAN, P.E.



(303) 442-4338



* ALL GEOLINK UNITS SHALL BE 6" HIGH (PETRAFLEX PRODUCT# PL61216) UNLESS NOTED OTHERWISE. CONSTRUCTION MUST BE IN ACCORDANCE WITH APPLICABLE CITY OF GREELEY CONSTRUCTION STANDARDS. THE CITY'S ACCEPTANCE ALLOWS FOR PLAN DISTRIBUTION AND PERMIT APPLICATION. THE CITY'S ACCEPTANCE SHALL NOT RELIEVE THE DESIGN ENGINEER'S RESPONSIBLITY FOR ERRORS, OMISSIONS, OR DESIGN DEFICIENCIES FOR WHICH, THE CITY IS HELD HARMLESS. 12/7/01 Date

Public Works Director

NO.

12/7/01 Water and Sewer Director

5.9

58.4

9.1

SIGNATURE AND DATE EW1139.

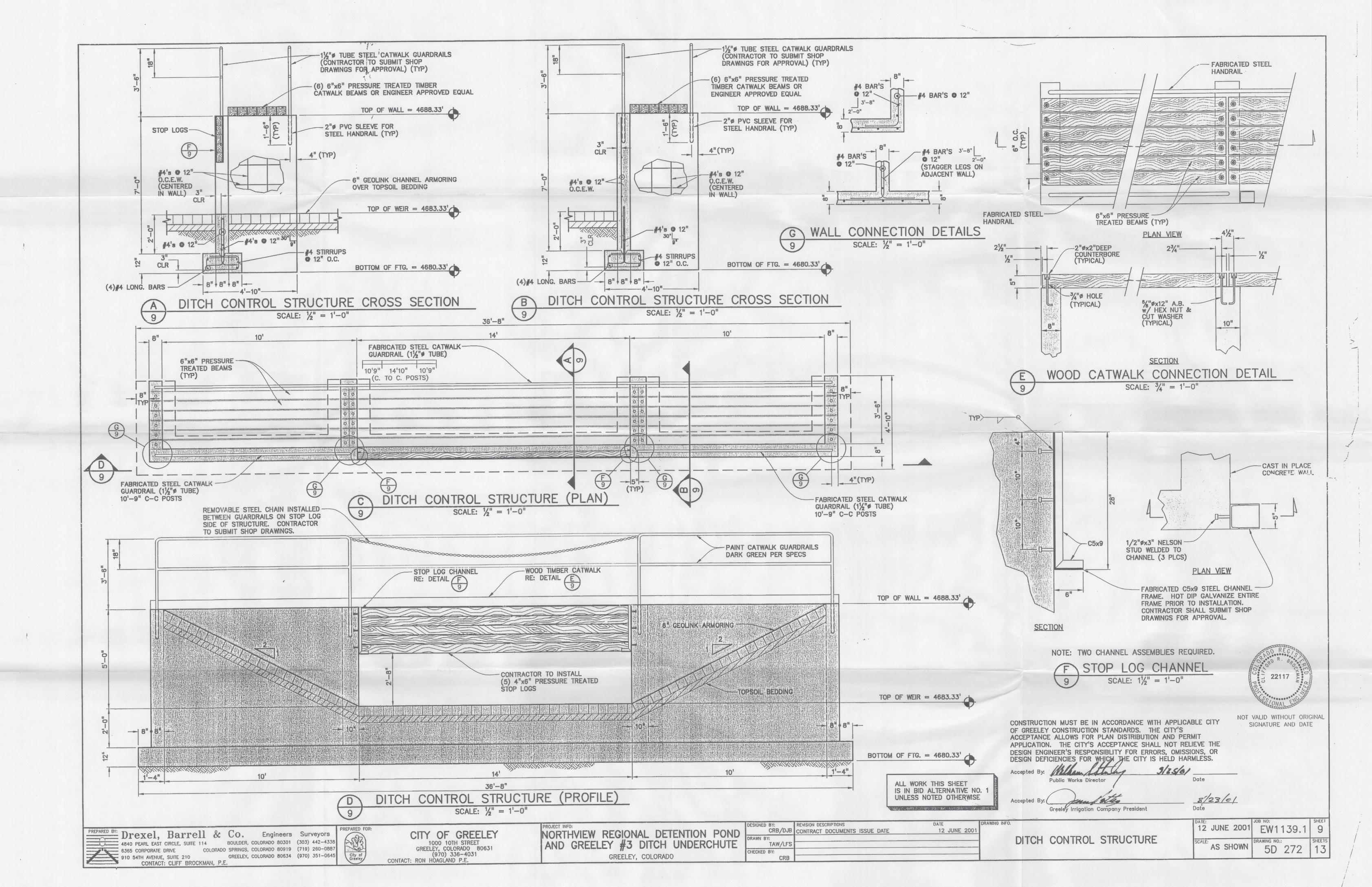
SHEET 1 OF//3

Greeley Irrigation Company President

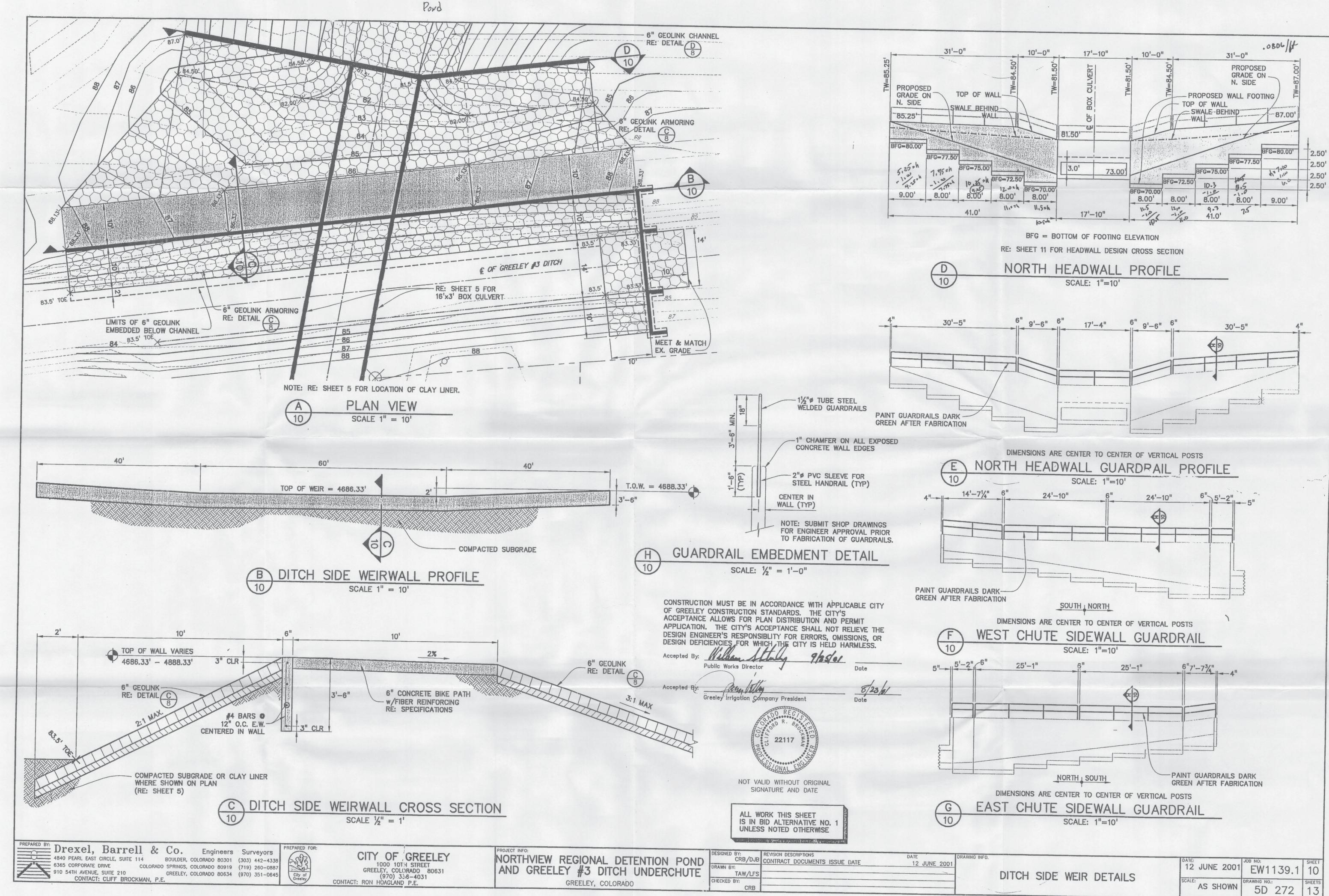
REVISED PIPE ALIGNMENT 30 NOV 2001

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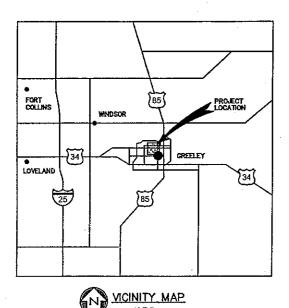


APPENDIX A.4 CLARKSON SPILL STRUCTURE

CLARKSON DIVERSION ON THE GREELEY NO. 3 DITCH GREELEY, COLORADO

CALL UTILITY NOTIFICATION CENTER OF COLORADO -800-922-1987

CALL 2-BUSINESS DAYS IN ADVANCE
BEFORE YOU DIG, GRADE, OR EXCAVATE FOR THE MARKING OF UNDERGROUND MEMBER UTILITIES.



N.T.S.

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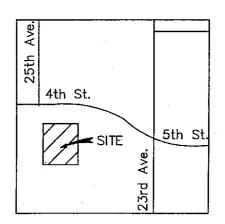
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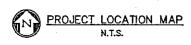
Barrell

9:22:

10/10/2003

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8 OCTOBER 2003

PREPARED FOR:

THE CITY OF GREELEY

1001 9th AVENUE GREELEY, COLORADO 80631 (970) 336-4121 CONTACT: BERT LEAUTAUD, P.E.

PREPARED BY:



Drexel, Barrell & Co. Engineers · Surveyors 4840 PEARL EAST CIRCLE, SUITE 114 BOULDER, COLORADO 80301 (303) 442-4338

> CONTACT: CLIFF BROCKMAN, P.E.

ESTIMATED QUANTITIES		
ITEM	UNIT	QTY
DEMO EXISTING STRUCTURE	LS	1
STRUCTURAL FILL	CY	65
STRUCTURAL CONCRETE	CY	*
CATWALKS, LADDER AND GUARDRAILS	SF	205
INSTALL CITY FURNISHED CMP (16 GA.) (ESTIMATED TO BE 36")	LF	20
FURNISH & INSTALL OVERSHOT GATE	LS	1
FURNISH & INSTALL CONTROL PEDESTAL W/ SOLAR POWER	LS	1
FURNISH & INSTALL 24"x24" SLIDE GATE	EA	1
FURNISH AND INSTALL STILLING WELL ASSEMBLING Y	EA	73.1
NON-STRUCTURAL BACKFILL	CY	51
CLEANUP AND DEMOBILIZATION	LS	1

	SHEET INDEX
SHEET NO.	SHEET DESCRIPTION
1	COVER SHEET
2	EXISTING STRUCTURE DEMOLITION PLAN
3	PROPOSED DIVERSION SITE PLAN
4	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS
5	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS
6	PROPOSED DIVERSION SECTIONS & STRUCTURAL DETAILS
7	CATWALK PLAN AND DETAILS
- 8	CATWALK, LADDER AND GUARDRAIL DETAILS
9	STILLING WELL AND ARMITEC POWER PEDESTAL DETAILS

ALL WORK S	HALL BE CONSTRUCTED TO THE CITY OF GREELEY STAND	_
APPROVED	CITY OF GREELEY DIRECTOR OF PUBLIC NORKS	10/24/03 DATE
APPROVED	CITY OF GLEELEY DIRECTOR OF WATER & SEWER	1 24 03 DATE
APPROVE:	THE CREELEY ARRIVATION COMPANY	10.29-0

STRUCTURAL NOTES

GENERAL REQUIREMENTS:

 A. ALL CONSTRUCTION SHALL COMPLY WITH THE 1997 UNIFORM BUILDING CODE, OR
 LATER ENTION ADOPTED BY THE GOVERNMENTAL JURISDICTION, AND ALL OTHER
 PERTINENT GOVERNMENTAL CODES, ORDINANCES AND REGULATIONS.

2. FOUNDATIONS: : A. DESIGN IS BASED ON A MAT SLAB FOUNDATION, PLACED ON 2 FEET OF COMPACTED STRUCTURAL FILL. MAXMUM BEARING PRESSURE USED IN DESIGN = 1000

PERC

PAIL

3. CUNCRETE:
A ALL CONCRETE SHALL COMPLY WITH THE LATEST EDITIONS OF THE ACT
SPECIFICATIONS FOR STRUCTURAL CONCRETE, ACT 301, AND ACT BUILDING CODE
REQUIREMENTS FOR REINFORCED CONCRETE, ACT 318.
B. CONCRETE MIX DESIGN, AIR ENTRAINMENT, PLACEMENT, TRANSPORT, ETC. SHALL BE
PER ACT SPECS. MIX DESIGN IS SUBJECT TO THE ENGINEER'S APPROVAL.
C. ALL CONCRETE SHALL BE MADE USING TYPE I/I CEMENT, WITH STONE AGGREGATE,
AND SHALL DEVELOPE A MINIMUM 28-DAY COMPRESSIVE STEENOTH OF 4000 psl.
D. MIX DESIGN SHALL HAVE THE FOLLOWING PROPERTIES:
MAXIMUM WATER/CEMENT RATIO:
SLUMP AT SLABS
SLUMP AT SLABS
SLUMP AT SLABS
SLUMP AT SLABS
ART SLABS

PERMITTED BY THE BATCH TICKET. CONCRETE AT PLACEMENT TIME WHICH DOES NOT MEET THE SPECIFIED SUMP OR AIR CONTENT SHALL BE REFUSED BY THE CONTRACTOR. F. ALL REINFORCING STEEL SHALL BE ASTM A615—GRADE 60. (INCLUDING #4 AND #5 BARS).

C. REINFORCING STEEL SHALL BE FABRICATED AND PLACED IN ACCORDANCE WITH THE ACI MANUAL OF STANDARD PRACTICE.

H. CONCRETE PLACED AGAINST EARTH: 3"

2) CONCRETE PLACED AGAINST EARTH: 3"

2) CONCRETE PLACED IN FORMS AND EXPOSED TO EARTH, WEATHER OR WATER (PRINCIPAL REINFORCEMENT): 2"

3) TIES AND STRENDS: 1 1/2"

I. NO SPLICES OR WELDING OF REINFORCEMENT SHALL BE MADE EXCEPT AS DETAILED OR AUTHORIZED BY THE ENGINEER. LAP SPLICES, WHERE PERMITTED, SHALL BE 24" MINIMUM LUNLESS OTHERWISE NOTED.

J. DETAIL BARS IN ACCORDANCE WITH THE LATEST EDITIONS OF THE ACI DETAILING MANUAL AND ACI BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE. PROVIDE ALL ACCESSORIES NECESSARY TO SUPPORT REINFORCING AT THE POSITIONS SHOWN ON THE PLANS OR AS NOTED ABOVE.

K. SHOP DRAWINGS SHALL BE SUBMITTED FOR APPROVAL, IN REPRODUCIBLE FORM, OF ALL REINFORCING STEEL PRIOR TO FABRICATION.

L. PROVIDE 2—#5 BARS WITH 2'—0" PROCECTION ACOUND ALL OPENINGS IN CONCRETE. IM. DOWELS FROM MAT SLABS TO WALLS AND COLUMNS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE IN THE FOOTINGS TAKES PLACE.

II. N. DOWELS FROM MAT SLABS TO WALLS AND COLUMNS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE IN THE FOOTINGS TAKES PLACE.

III. N. DOWELS FROM MAT SLABS TO WALLS AND COLUMNS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE IN THE FOOTINGS TAKES PLACE.

III. N. DOWELS FROM MAT SLABS TO WALLS AND COLUMNS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE IN THE FOOTINGS TAKES PLACE.

III. N. DOWELS FROM MAT SLABS TO WALL SAND COLUMNS SHALL BE INSTALLED PRIOR TO FLACEMENT OF CONCRETE BARS AT ALL WALL INTERSECTIONS. SIZE AND SPACING OF BARS SHALL WALL MATCH HORIZONTAL WALL REINFORCING. DO NOT PLACE CORNER BARS FROM "INSIDE FACE TO INSIDE FACE". PROVIDE TORS FOR "INSIDE FACE TO INSIDE FACE". PROVIDE TOR CONCRETE AGAINT MOSTURE, PR

4. STEEL:

A. ALL STRUCTURAL STEEL SHALL CONFORM TO ASTM A36, UNLESS OTHERWISE
NOTED. STEEL PIPE SHALL CONFORM TO ASTM A53, CRADE B.
B. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN
ACCORDANCE WITH THE LATEST EDITIONS OF THE AISC MANUAL OF STEEL
CONSTRUCTION—ALLOWABLE STRESS DESIGN, AND AISC CODE OF STANDARD PRACTICE.

S. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FIELD VERIFY ALL DIMENSIONS AND TO IMMEDIATELY NOTIFY THE ENGINEER OF ANY DISCREPANCIES, CONDITIONS NOT SHOWN OR THAT WHICH DIFFER FROM THOSE SHOWN ON THE DRAWINGS.

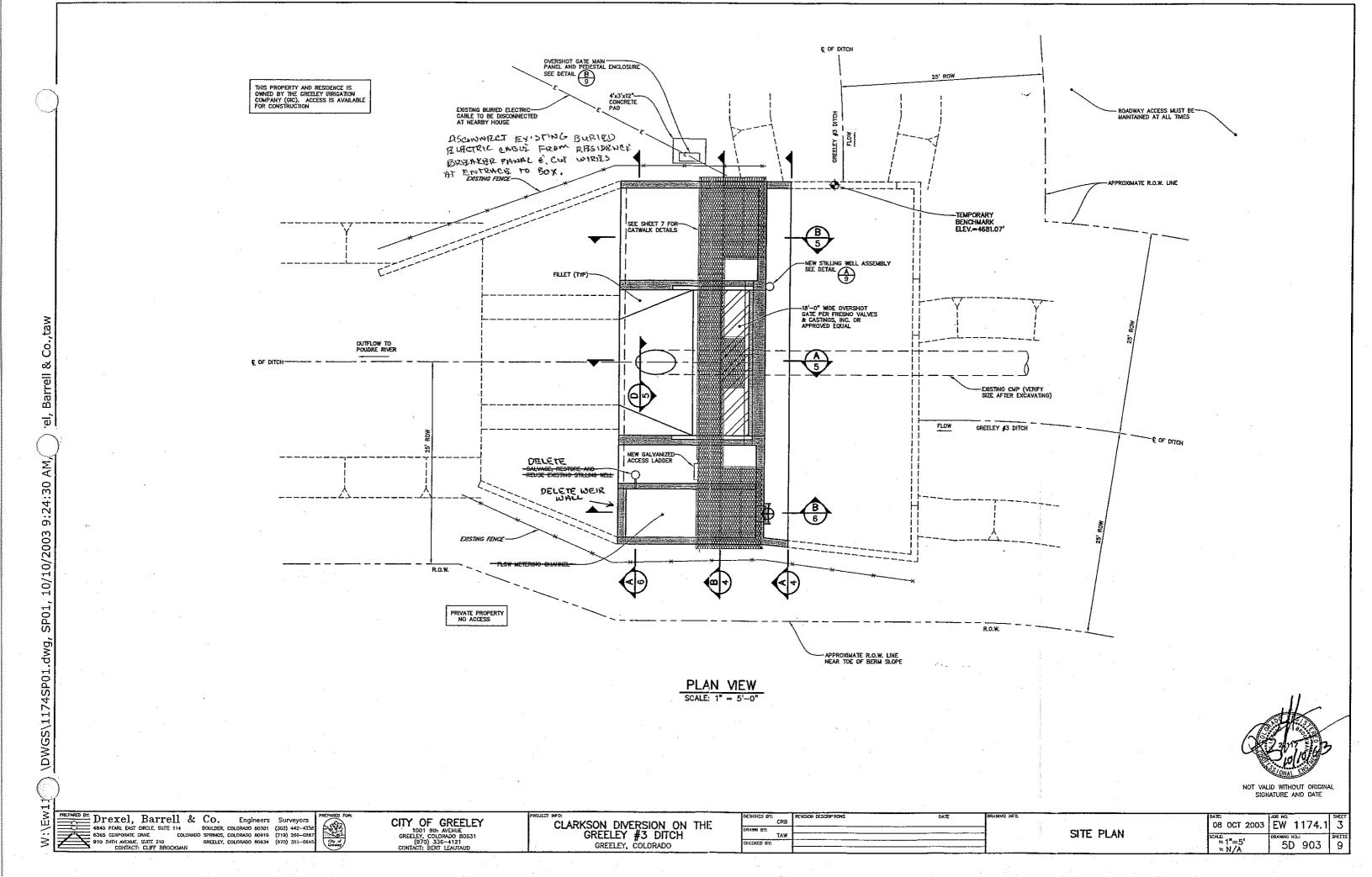
6. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING A SAFE WORKING ENVIRONMENT FOR ALL TRADES, AND FOR COMPLIANCE WITH ALL OSHA AND SAFETY RELATED REGULATIONS.

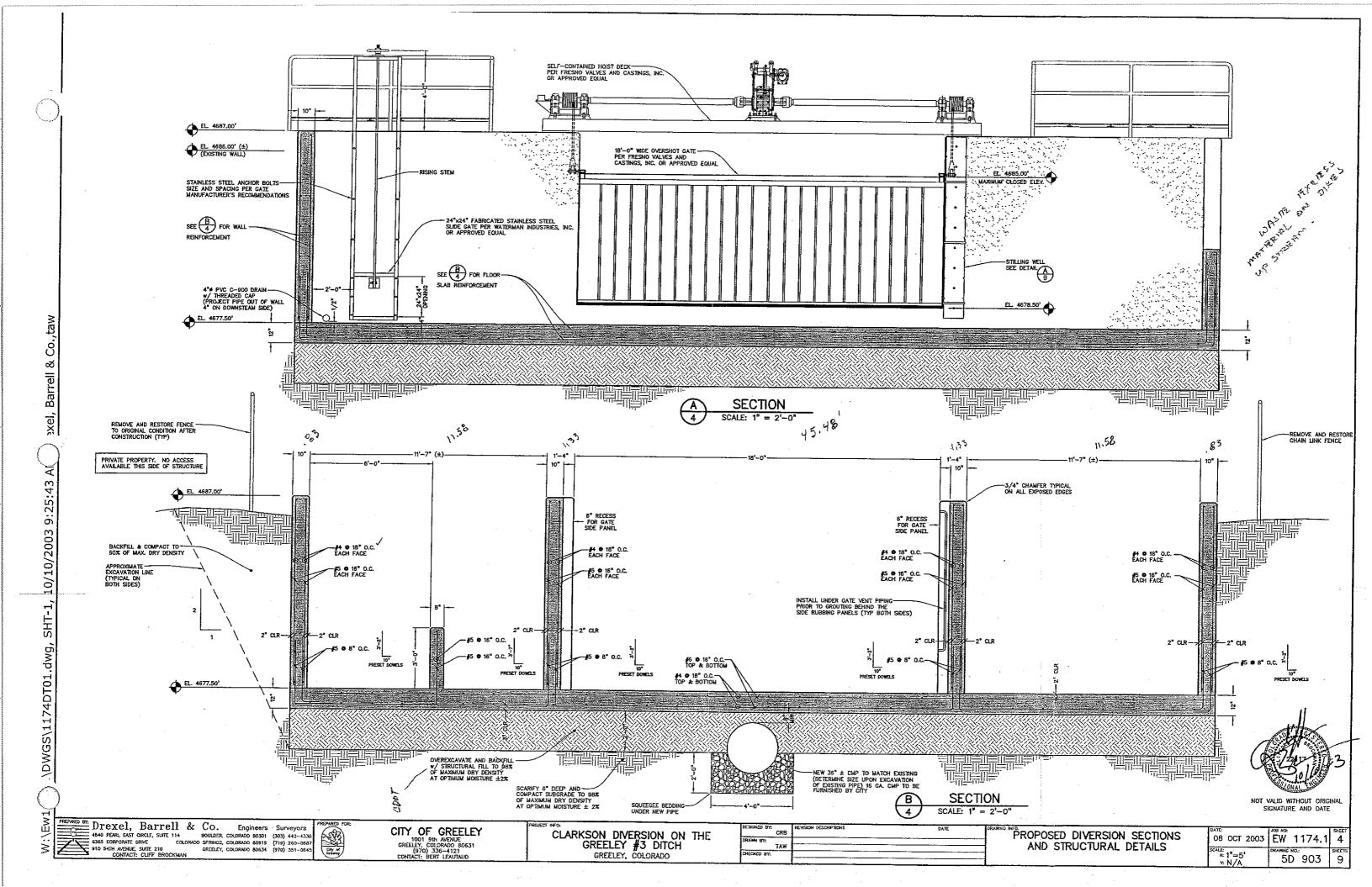


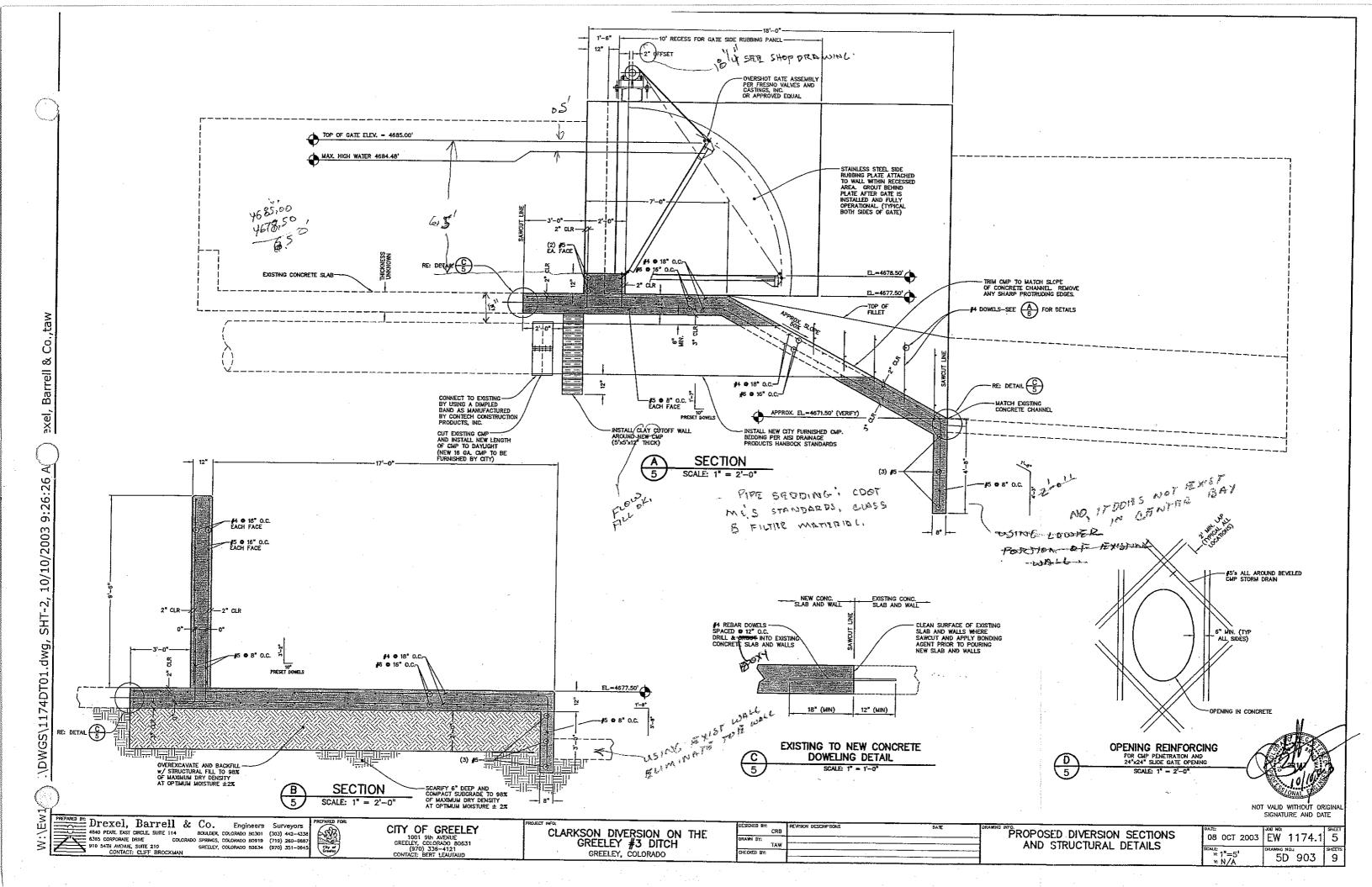
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DATE

5D 903 EW 1174.1 SHEET 1 OF 9







APPENDIX B

ELECTRONIC FILES: UNSTEADY FLOW HYDRAULIC MODELS [HEC-RAS VERSIONS 3.1.2 (EXISTING CONDITION) AND 3.1.3 (PROPOSED CONDITION)]